

Correlated Noise Modeling - An Implementation into HICUM

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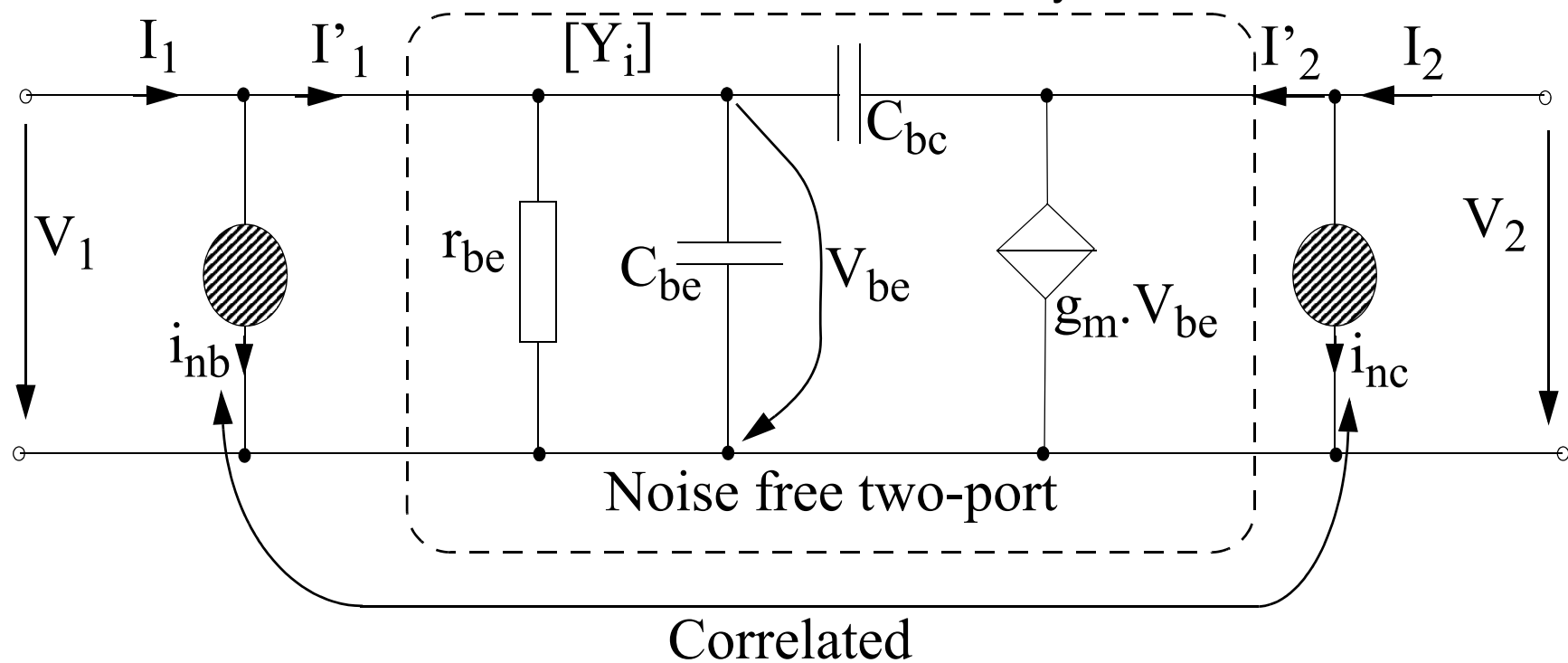
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Outline

- Correlated Noise in HBTs
- PSD matrix : problems with SPICE
- System theoretical solution
- Implementation challenges
- Implementation into HICUM
- Results

Correlated Noise in HBTs

- Presently in HICUM: thermal noise, shot noise, flicker noise
- Base and collector shot noise sources are actually correlated



PSD matrix: problems with SPICE

- Output noise power spectral density

$$S_{YY}(j\omega) = G(j\omega) \cdot S_{XX}(j\omega) \cdot G^+(j\omega)$$

- $S_{XX}(j\omega)$: input noise power spectral density
- $G(j\omega)$: transfer function matrix, $G^+(j\omega)$: complex conjugate of $G(j\omega)$

$$S_{XX}(j\omega) = \begin{bmatrix} S_{i_{nb}} & S_{i_{nb}i_{nc}} \\ S_{i_{nc}i_{nb}} & S_{i_{nc}} \end{bmatrix}$$

- Cross-correlated terms
 - Off-diagonal elements
 - not handled by SPICE simulators
 - crucial from operating frequencies around and above $f_{Tpeak}/10$

System theoretical solution

- Manipulate input noise PSD matrix

$$S_{XX}(j\omega) = T(j\omega) \cdot S_{\bar{X}}^N(j\omega) \cdot T^+(j\omega) \quad S_{\bar{X}}^N(j\omega) = \begin{bmatrix} S_{i_{nb}}^N & 0 \\ 0 & S_{i_{nc}}^N \end{bmatrix} \quad T(j\omega) = \begin{bmatrix} 1 & 0 \\ t_{21} & 1 \end{bmatrix}$$

$$S_{YY}(j\omega) = G(j\omega) \cdot T(j\omega) \cdot S_{\bar{X}}^N(j\omega) \cdot T^+(j\omega) \cdot G^+(j\omega)$$

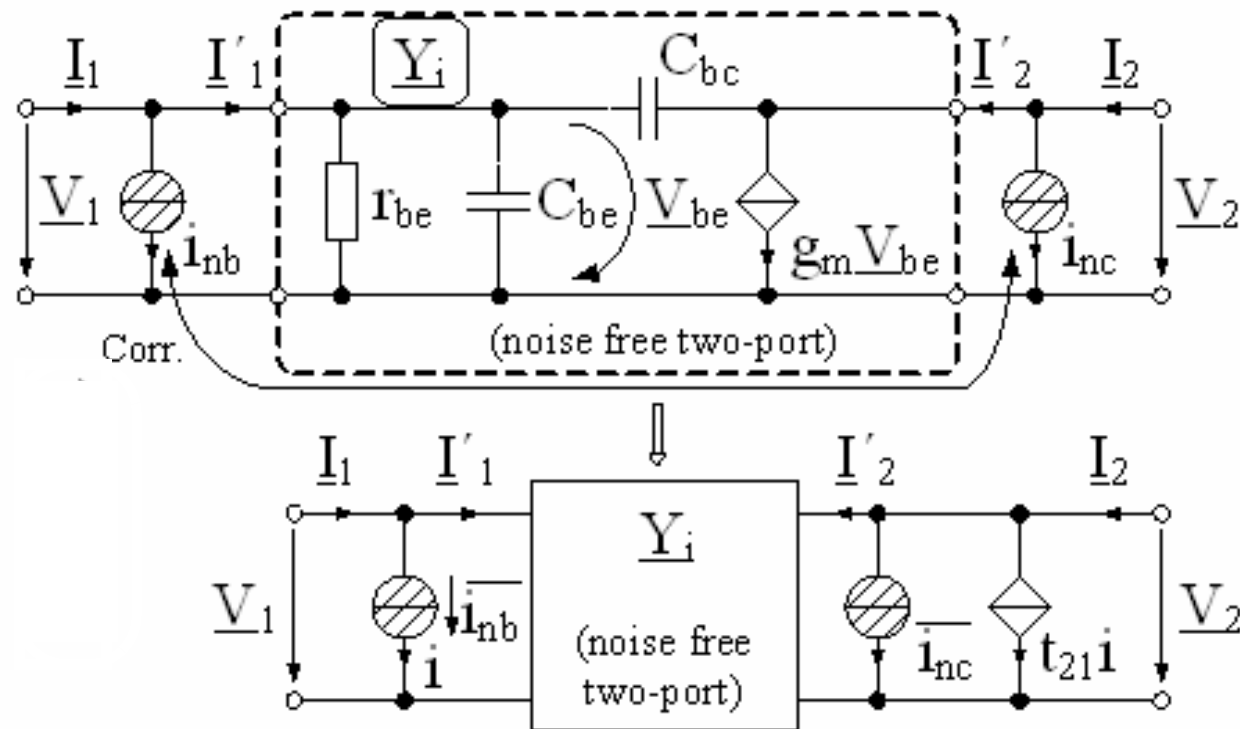
- Cross-correlated terms inside the transfer function
- From matrix element comparison

$$S_{i_{nb}}^N = S_{i_{nb}} \quad S_{i_{nc}}^N = S_{i_{nc}} - S_{i_{nb}} |t_{21}|^2$$

and

$$t_{21} = \frac{S_{i_{nc}i_{nb}}}{S_{i_{nb}}} = \frac{-2qI_C(j\omega\tau_B/3)}{2qI_B} = -j\omega \frac{\tau_B}{3} \frac{I_C}{I_B}$$

System theoretical solution (cont'd)



- Original noise PSD matrix: two correlated noise sources
- After manipulation: three uncorrelated noise sources with different PSDs

Implementation challenges

- Problem at first look
 - frequency dependent PSD at output

$$S_{i_{nc}}^N = S_{i_{nc}} \left(1 - \beta_{dc} \left(\frac{\omega \tau_B}{3} \right)^2 \right) \quad S_{i_{new}}^N = \left| \omega \frac{\tau_B}{3} \beta_{dc} \right|^2 S_{i_{nb}}$$

- solution
 - time derivative of noise source: operator " $ddt()$ " produces " $j\omega$ " in frequency domain
- Further problem
 - negative sign inside PSD
 - impossible by simple addition/subtraction of noise sources
 - addition/subtraction of noise PSD not possible
 - multiplication of noise sources not permitted in SPICE

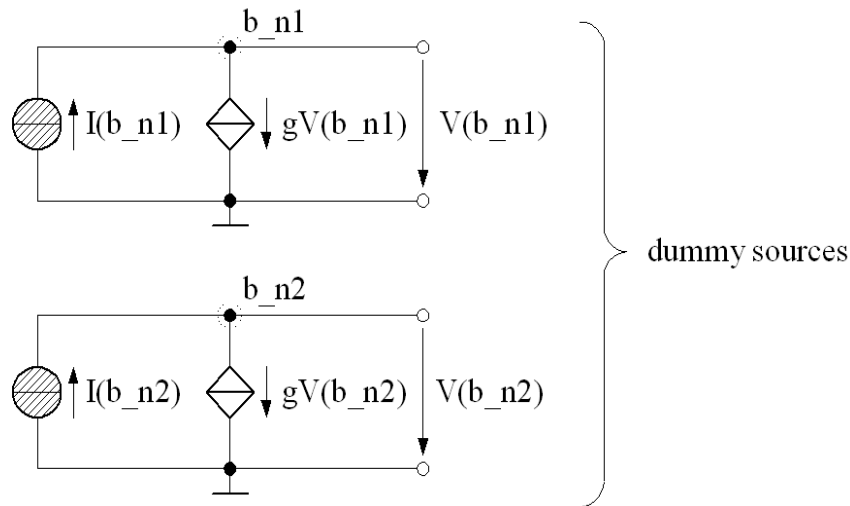
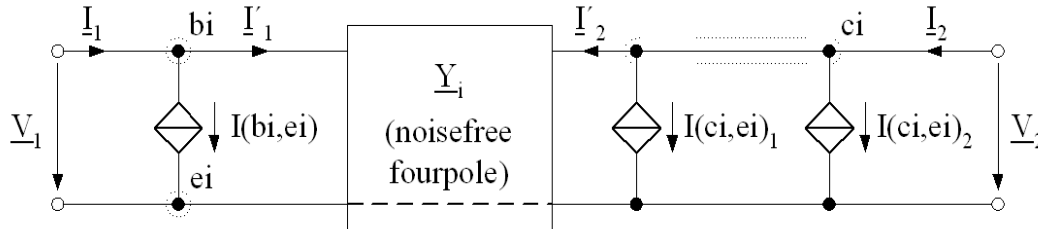
Implementation into HICUM

- One source at input side: same as before
- Two sources at output side
 - one requires derivative w.r.t. time of the input noise source
 - for the remaining one, following PSD proposed

$$S_{i_{nc}}^N = S_{i_{nc}} \left(1 - \frac{\beta_{dc}}{2} \left(\frac{\varpi \tau_B}{3} \right)^2 \right)^2 = S_{i_{nc}} \left(1 - \beta_{dc} \left(\frac{\varpi \tau_B}{3} \right)^2 + \left(\frac{\beta_{dc}}{2} \left(\frac{\varpi \tau_B}{3} \right)^2 \right)^2 \right)$$

- Last term reflects the error
 - for this PSD, accurate upto $f_{Tpeak}/3$
 - combining all PSDs, accurate upto f_{Tpeak}
 - very small in all practical purposes

Implementation into HICUM (cont'd)



- Time derivative: capacitive
- Total transit time used
- Incorporated into HICUM
- simulated with ADS 2004A
- Tested against 150GHz HBT

- Source 1:

$$I(bi,ei) = g \cdot V(b_n1)$$

$$V(b_n1) = \frac{1}{g} \sqrt{2qI_B}$$

- Source 3:

$$I(ci,ei)_2 = \beta_f k \tau_f \frac{d}{dt} (-g \cdot V(b_n1))$$

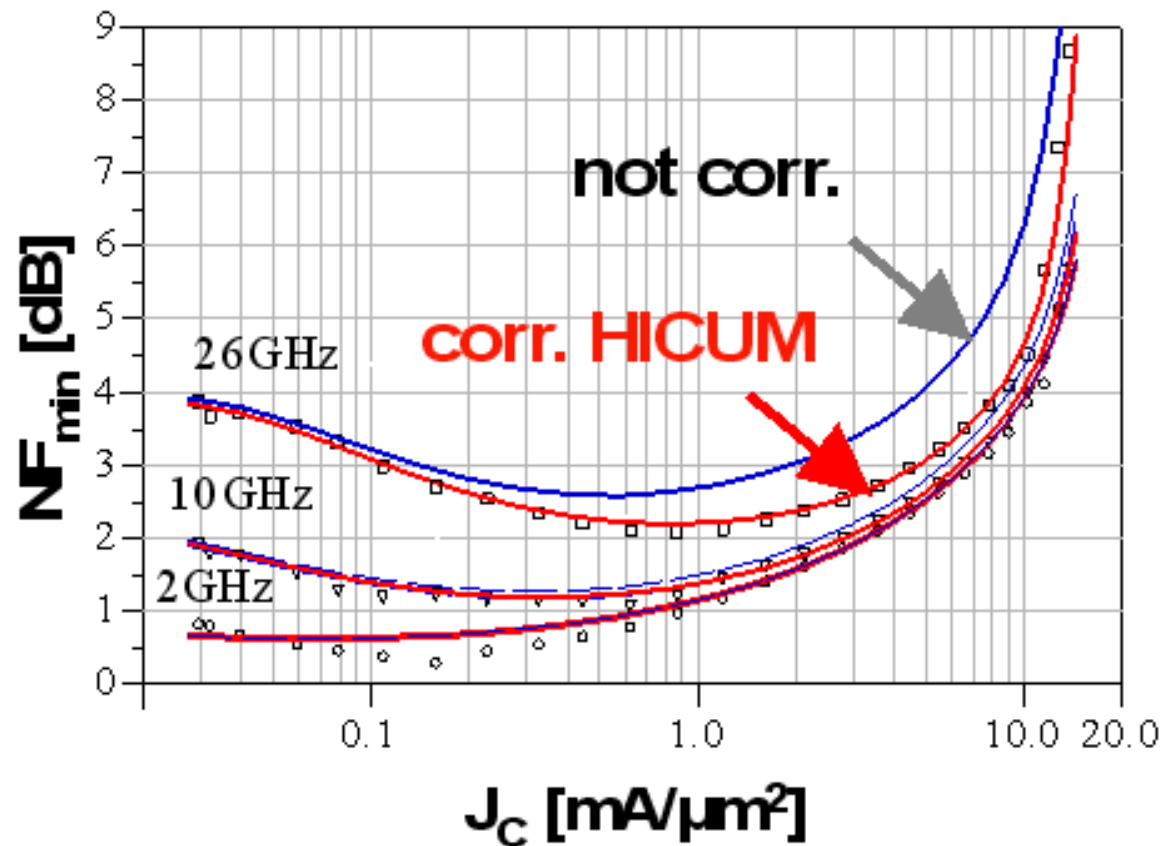
- Source 2:

$$I(ci,ei)_1 = g \cdot V(b_n2) + \frac{\beta_f}{2} (k \tau_f)^2 \frac{d^2}{dt^2} (g \cdot V(b_n2)) \quad V(b_n2) = \frac{1}{g} \sqrt{2qI_C} \quad , \quad g : 1 \text{ Siemens}$$

Results

$$T=300\text{K}, A_E=(0.2 \times 10.16)\mu\text{m}^2, V_{CE}=1.5\text{V}$$

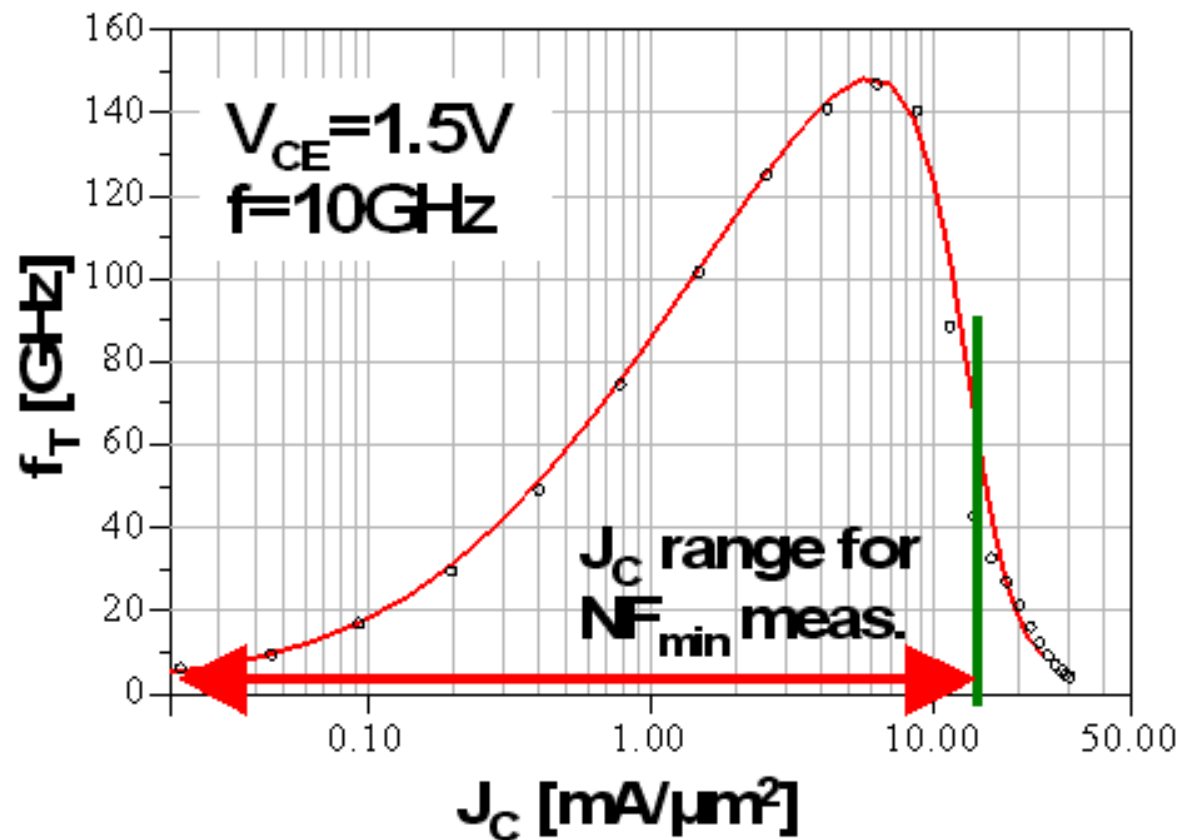
measurement: symbols, simulation: lines



Results (cont'd)

$$T=300\text{K}, A_E=(0.2 \times 10.16)\mu\text{m}^2$$

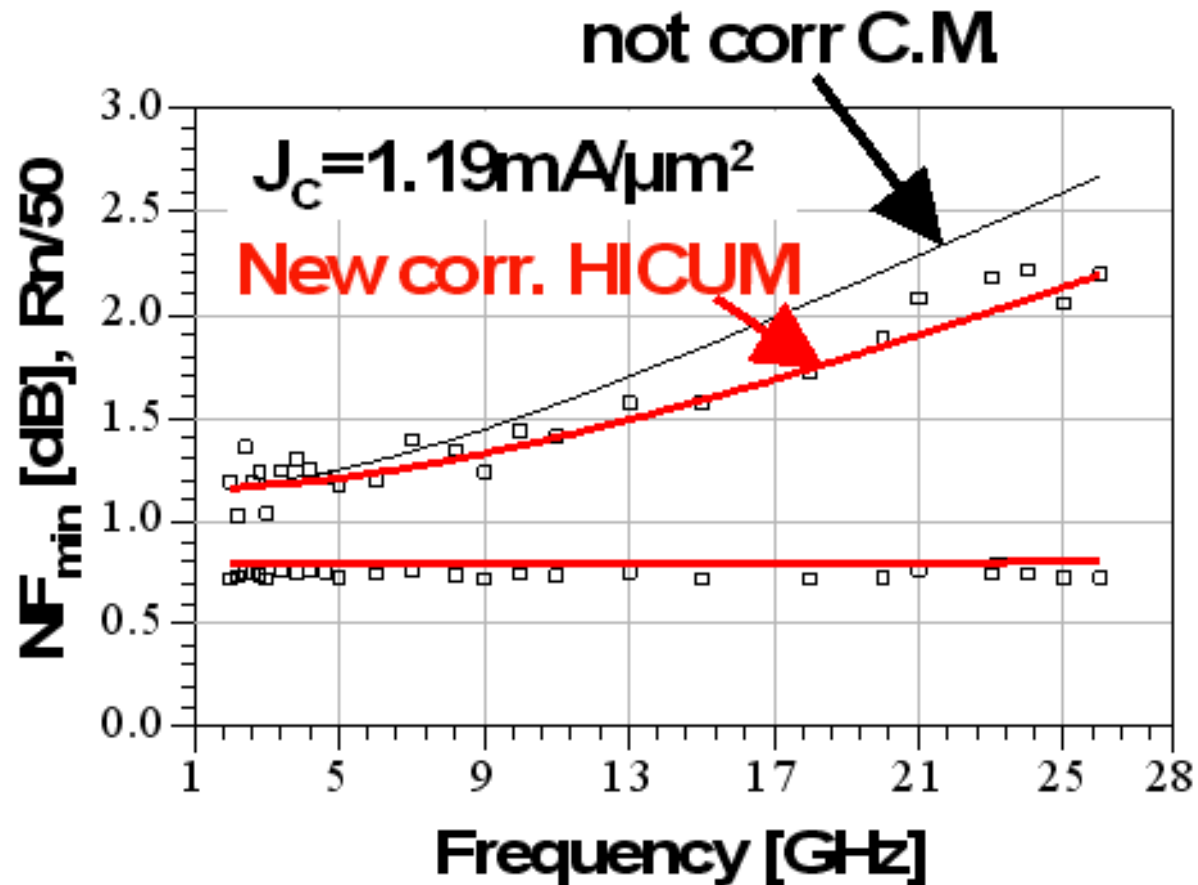
measurement: symbols, simulation: lines



Results (cont'd)

$T=300\text{K}$, $A_E=(0.2 \times 10.16)\mu\text{m}^2$, $V_{CE}=1.5\text{V}$, $J_C=2.74\text{mA}/\mu\text{m}^2$

measurement: symbols, simulation: lines



Conclusions

- Relevance of modeling noise correlation in modern HBTs discussed
- SPEICE-specific implementation problems pointed out
- A system theoretical solution proposed
- Corresponding Verilog-A implementation challenges discussed
- Implemented in HICUM and verified with measured data from advanced HBT ($f_{Tpeak}=150$ GHz) process

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