

About Modeling the Reverse Early Effect in HICUM Level 0

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Purpose

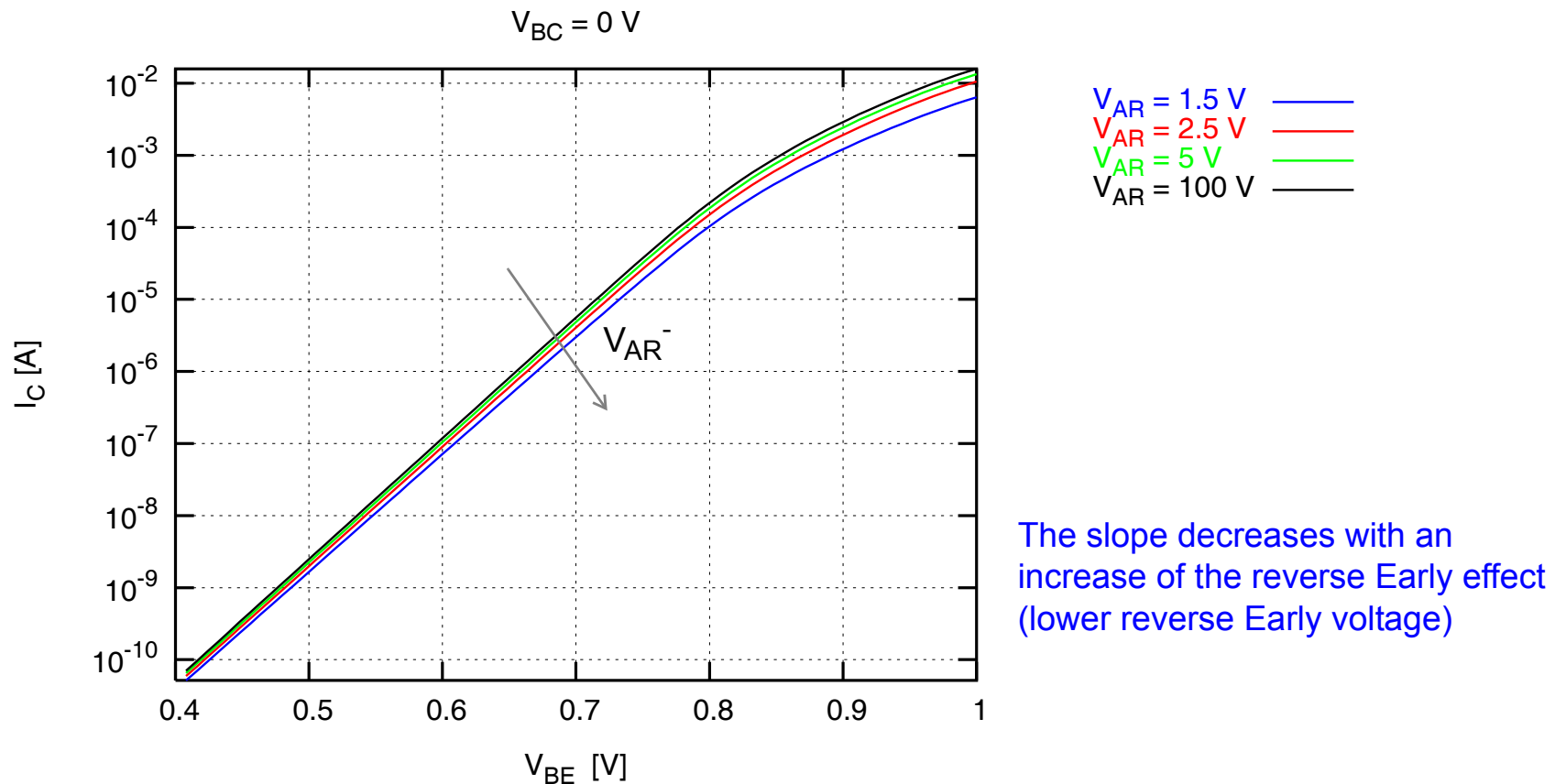
- According to the bipolar models, the reverse Early effect is modeled in various ways
 - From device physics in models such as HICUM, MEXTRAN or VBIC.
 - With more or less important approximations for models like SPICE Gummel-Poon (SGP) or HICUM Level 0.
- The question is to know if these approximations are justified and which are their impacts on the model accuracy.
- Application to HICUM/L0

Outline

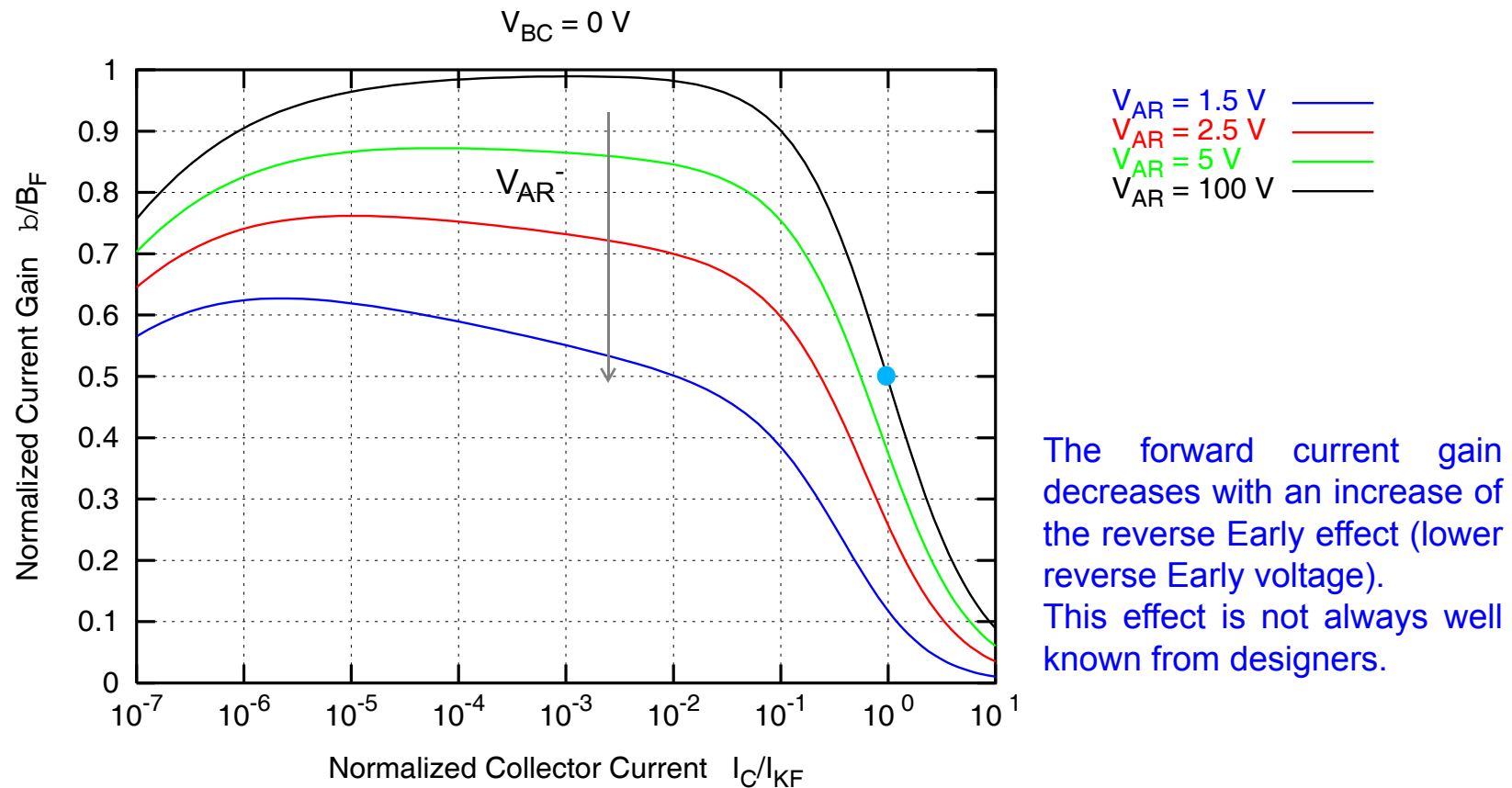
- Introduction
- Why Reverse Early effect is so important?
- How is it implemented in BJT models?
- Experimental results and HICUM/L0 limitation
- Summary

Introduction

- Despite its name, the *reverse* Early effect affects strongly the collector current in *forward* mode.
- Difficult to observe on forward Gummel plots, its effect being concealed by the exponential dependence of I_C with V_{BE}

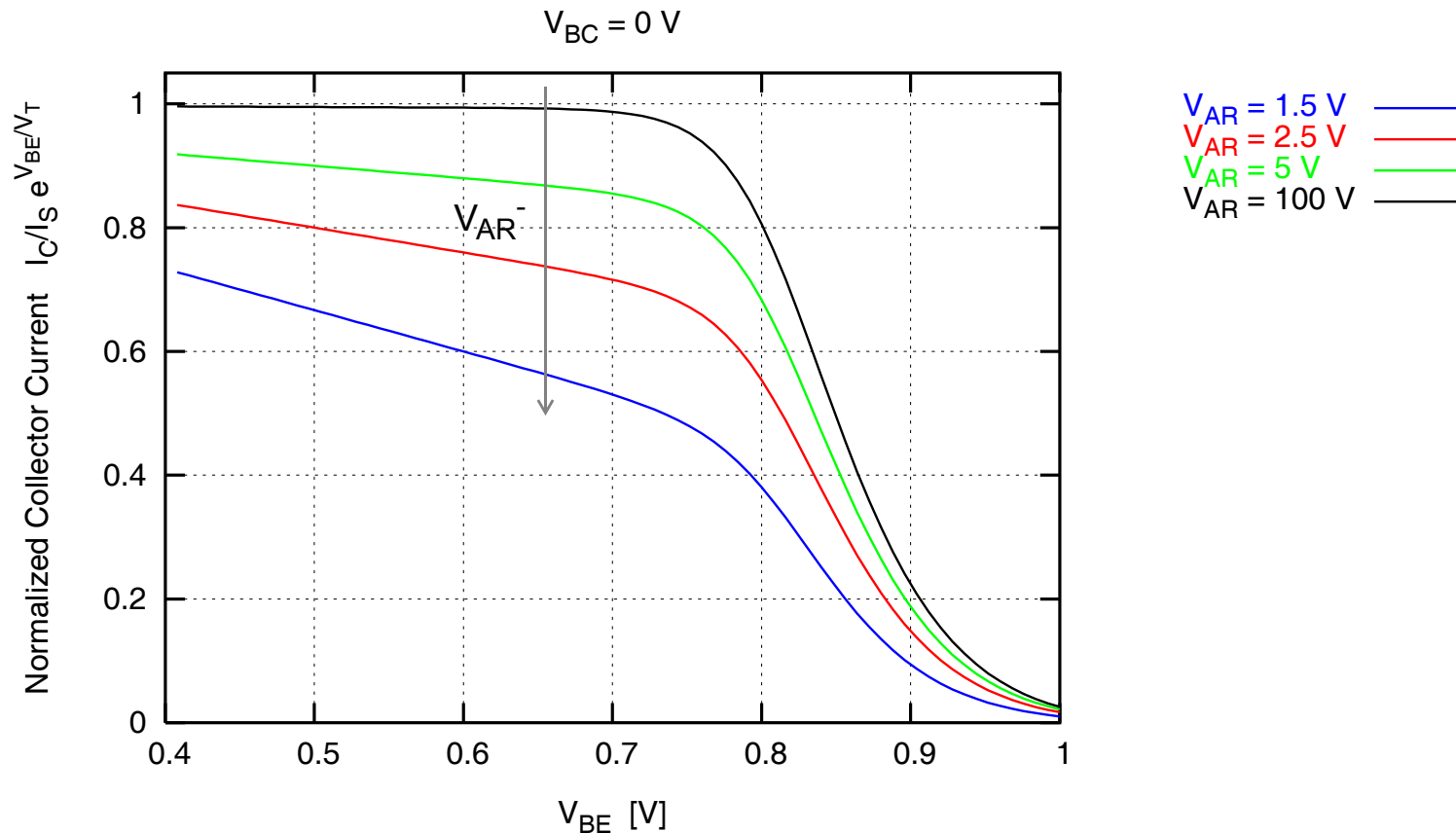


→ But clearly visible on the forward current gain...



- We can observe that the forward current gain is divided by 2 at $I_C = I_{KF}$. It is a way to directly extract the forward knee current I_{KF} of the SGP model, from the forward current gain corrected of the reverse Early effect.

→ ...or better on the *normalized* collector current $I_C/I_S e^{V_{BE}/V_T}$



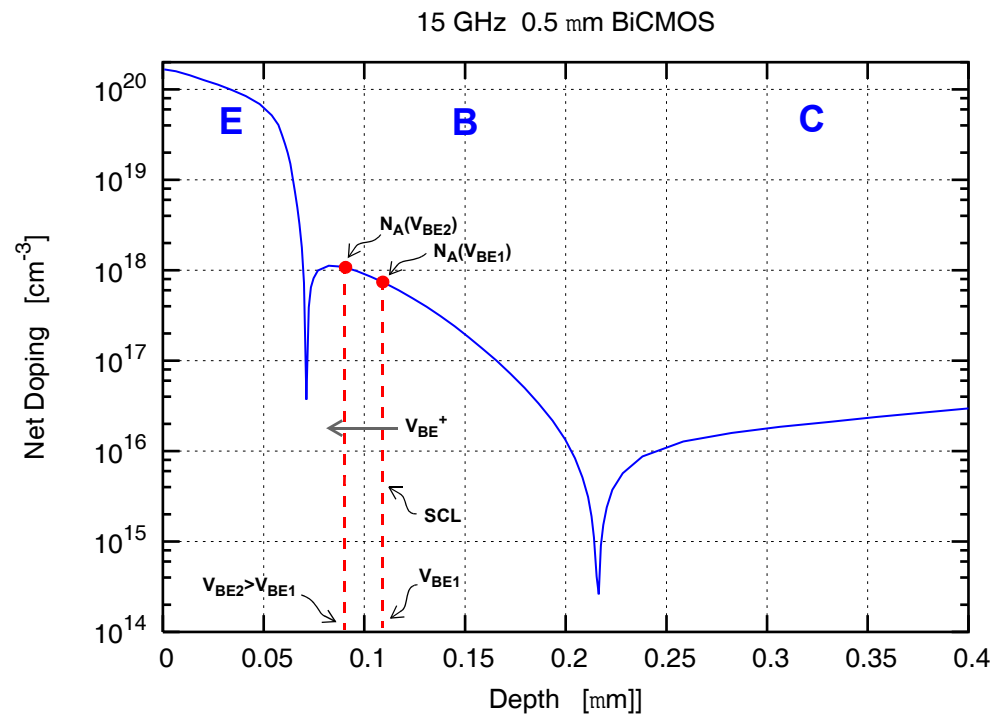
- We can notice, that in fact this *normalized* collector current is, at low and medium V_{BE} (linear part of the characteristic), simply the inverse of the normalized hole charge Q_p/Q_{p0} .
- The reverse Early effect can be directly quantified from the slope of this *normalized* collector current.
- It is the only way to directly extract (linear regression), without any ambiguity, the reverse Early voltage V_{AR} of the SGP model.

Why the Reverse Early Effect so Important?

- Whatever the technology, for vertical (conventional) BJTs, the reverse Early effect is not negligible (low equivalent reverse Early voltage on the order of 1 to 5V). Why?
- Initially, the inverse Early voltage V_{AR} was introduced, in the SGP model, in order to take into account the base width modulation with V_{BE} .
- In fact, in advance bipolar technologies, the base doping is very high, and consequently, the base width is less affected by a V_{BE} variation.
- Therefore, low reverse Early voltages, for this kind of technologies, can not be explained only by a modulation of the base resulting from a variation of the BE space-charge layer width.
- 2 possible explanations
 - The reverse Early voltage does not depend only on the base concentration, but also on the shape of the base doping (Si BJTs).
 - Reverse (effective) Early voltage can be also effected by the Ge profile in the base of HBTs.

Effect of the Shape of the Base Doping on $I_C(V_{BE})$

→ Si BJTs



- The collector current depends on the injected electron in the base, at the EB depletion layer boundary

$$I_C \propto n_{b0}(V_{BE}) \cdot e^{\frac{V_{BE}}{V_T}} \quad \text{or} \quad I_{C^*} = \frac{I_C}{e^{\frac{V_{BE}}{V_T}}} \propto n_{b0}(V_{BE})$$

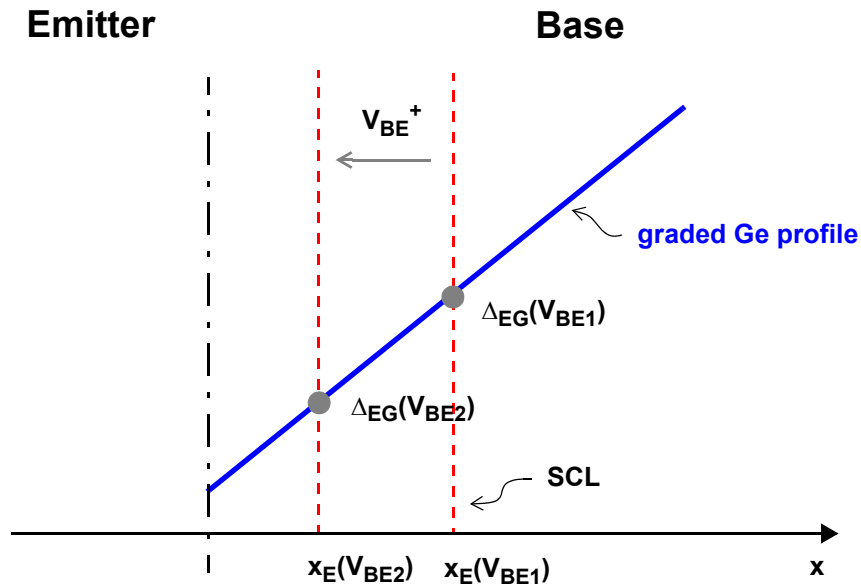
- If V_{BE} increases $N_A(V_{BE2}) > N_A(V_{BE1})$
- Since $n_{b0} \approx \frac{n_i^2}{N_A}$, we have $n_{b0}(V_{BE2}) < n_{b0}(V_{BE1})$

and therefore $I_{C^*}(V_{BE2}) < I_{C^*}(V_{BE1})$

- Similar effect than the reverse Early effect (base width modulation with V_{BE}), where I_{C^*} decreases with V_{BE} .

Effect of the Ge Base Profile on the $I_C(V_{BE})$

→ HBTs



- In HBTs, the collector current depends on the reduction Δ_{EG} of the base bandgap due to the introduction of Ge into the base

$$I_{C^*} = \frac{I_C}{e^{V_{BE}/V_T}} \propto e^{\frac{\Delta_{EG}}{V_T}}$$

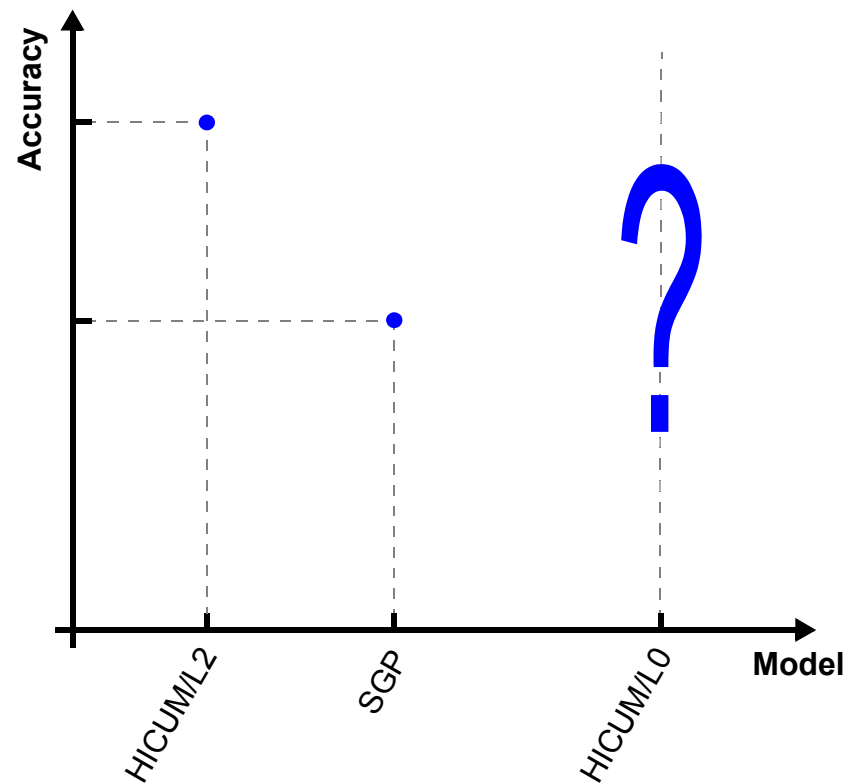
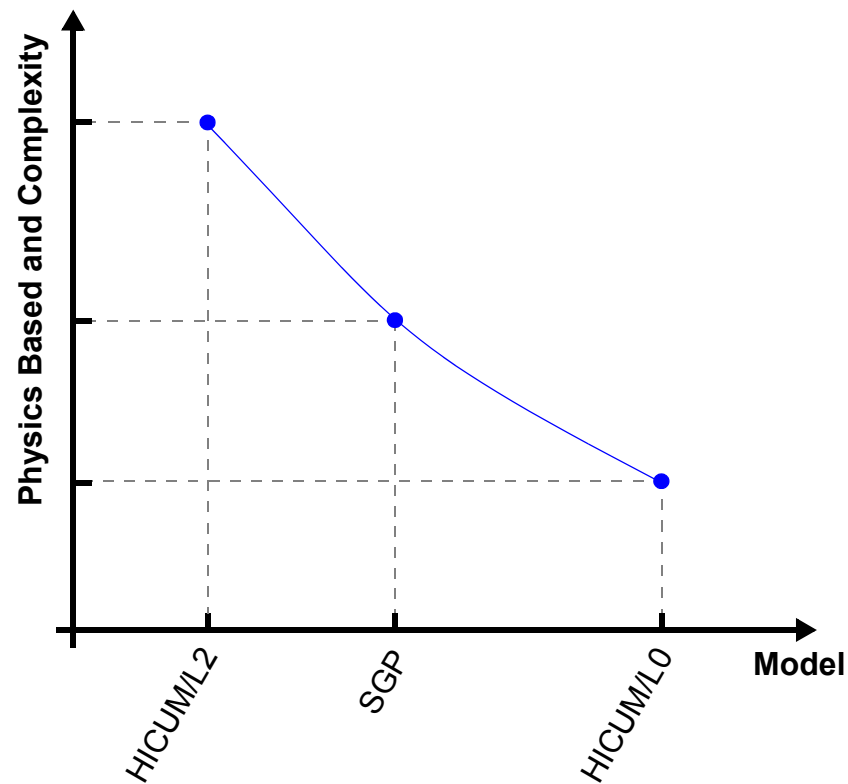
- In graded Ge base profile (triangle or trapezoidal), if V_{BE} increases $\Delta_{EG}(V_{BE2}) < \Delta_{EG}(V_{BE1})$

and therefore $I_{C^*}(V_{BE2}) < I_{C^*}(V_{BE1})$

- This effect is responsible of the very low *effective* reverse Early voltage (decrease of I_{C^*} with V_{BE}) of S_iG_e HBTs with graded Ge base profile.

How the Reverse Early Effect is Implemented in BJT Models?

→ Depending on the model, several approaches more or less physics based



→ HICUM Level 2

- Low injection, $V_{BC} = 0 \text{ V}$

$$I_C \approx \frac{I_S \cdot e^{\frac{V_{BEi}}{V_T}}}{1 + h_{jEi} \cdot \frac{Q_{jEi}}{Q_{p0}}} = \frac{I_S \cdot e^{\frac{V_{BEi}}{V_T}}}{1 + h_{jEi} \cdot q_{jEi}}$$

h_{jEi} weighting factor in HBTs

q_{jEi} normalized BE depletion charge

→ SPICE Gummel-Poon

- Low injection, $V_{BC} = 0 \text{ V}$

$$q_{jEi} = \frac{1}{Q_{p0}} \cdot \int_0^{V_{BEi}} C_{jEi}(V) \, dV$$

In SGP model, C_{jEi} is assumed to be constant and equal to its average value $\overline{C_{jEi}}$

$$I_C \approx \frac{I_S \cdot e^{\frac{V_{BEi}}{V_T}}}{1 + h_{jEi} \cdot q_{jEi}} \approx \frac{I_S \cdot e^{\frac{V_{BEi}}{V_T}}}{1 + \frac{h_{jEi} \cdot \overline{C_{jEi}} \cdot V_{BEi}}{Q_{p0}}} = \frac{I_S \cdot e^{\frac{V_{BEi}}{V_T}}}{1 + \frac{V_{BEi}}{V_{AR}}} \quad \text{with } V_{AR} = \frac{Q_{p0}}{h_{jEi} \cdot \overline{C_{jEi}}}$$

- Moreover, In SGP model it is assumed (questionnable for advanced HBTs) $V_{AR} \gg V_{BEi}$

$$1 / \left\{ 1 + \frac{V_{BEi}}{V_{AR}} \right\} \approx 1 - \frac{V_{BEi}}{V_{AR}}, \text{ and finally } I_C \approx \left\{ 1 - \frac{V_{BEi}}{V_{AR}} \right\} \cdot I_S \cdot e^{\frac{V_{BEi}}{V_T}}$$

→ HICUM Level 0

- Low injection, $V_{BC} = 0$ V

Same approximation than in SGP model, it is assumed that $V_{AR} \gg V_{BEi}$.

Therefore $1 - \frac{V_{BEi}}{V_{AR}}$ can be considered as the first two terms of the Taylor series expansion of $e^{-\frac{V_{BEi}}{V_{AR}}}$

$$I_C \approx \left\{ 1 - \frac{V_{BEi}}{V_{AR}} \right\} \cdot I_S \cdot e^{\frac{V_{BEi}}{V_T}} \approx I_S \cdot e^{-\frac{V_{BEi}}{V_{AR}}} \cdot e^{\frac{V_{BEi}}{V_T}} = I_S \cdot e^{\frac{V_{BEi}}{V_T} \cdot \left\{ 1 - \frac{V_T}{V_{AR}} \right\}}$$

We can consider $V_T/V_{AR} \ll 1$, $1 - \frac{V_T}{V_{AR}}$ can be rewritten as $1 - \frac{V_T}{V_{AR}} \approx 1 / \left\{ 1 + \frac{V_T}{V_{AR}} \right\}$,

which gives the final expression of I_C

$$I_C \approx I_S \cdot e^{\frac{\frac{V_{BEi}}{\left\{ 1 + \frac{V_T}{V_{AR}} \right\} \cdot V_T}}{}} = I_S \cdot e^{\frac{V_{BEi}}{M_{CF} \cdot V_T}} \quad \text{with} \quad M_{CF} = 1 + \frac{V_T}{V_{AR}}$$

→ Few comments concerning the relation between M_{CF} and V_{AR}

- As $M_{CF} = 1 + \frac{V_T}{V_{AR}}$ and $V_{AR} \gg V_T$

therefore M_{CF} is very close to 1. In order to reproduce accurately the reverse Early effect, M_{CF} must be given at least with **5 digits**.

V_{AR} (V)	M_{CF}
1.5	1.01724279
2.5	1.01034567
5	1.00517284
100	1.00025864

M_{CF} (4 digits)	V_{AR} (V)
1.017	1.5 21
1.010	2.5 86
1.005	5. 173
1.000	∞

M_{CF} (5 digits)	V_{AR} (V)
1.0172	1.5 04
1.0103	2.5 11
1.0051	5.0 71
1.0002	129.32

- As $M_{CF} = 1 + \frac{V_T}{V_{AR}}$, it *could be* temperature dependant (assuming V_{AR} temperature independent).

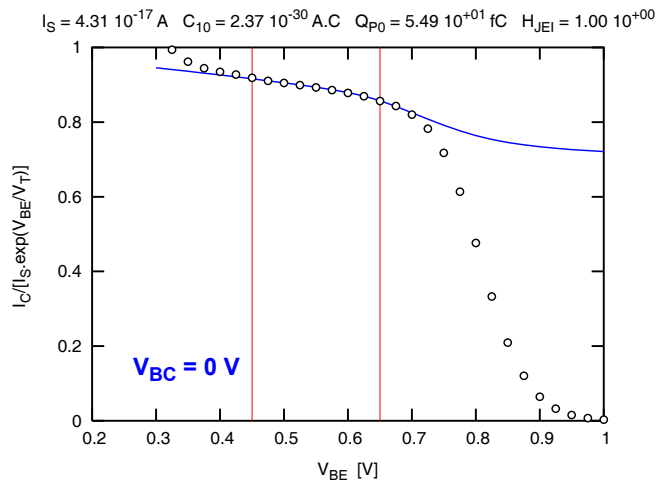
To be investigated in more detail (to a next HICUM workshop!...)

Temperature (°C)	V_{AR} (V)	M_{CF}
-50	2.5	1.00769
27	2.5	1.01034
150	2.5	1.01458

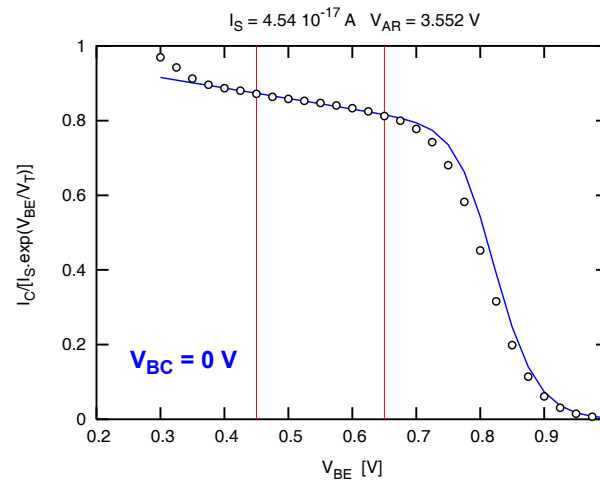
Experimental Results

→ HICUM/L2, SGP, HICUM/L0 ¹

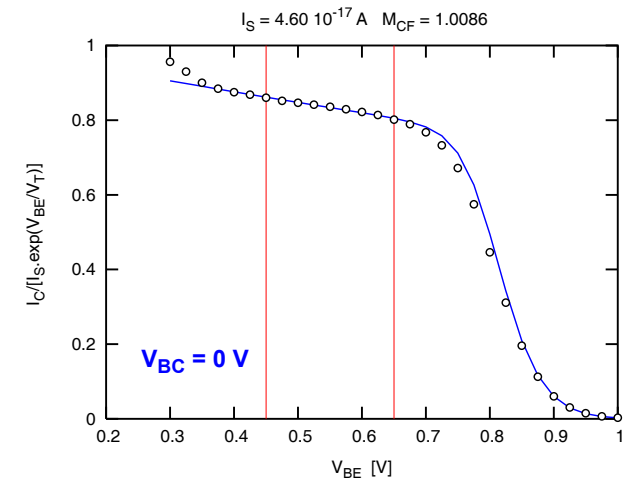
- High current parameters not fully extracted



HICUM/L2



SGP

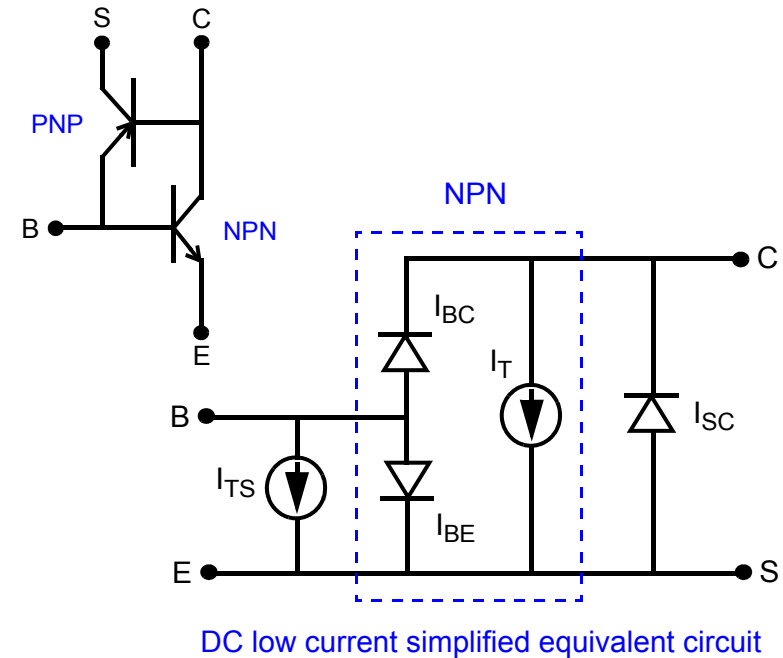
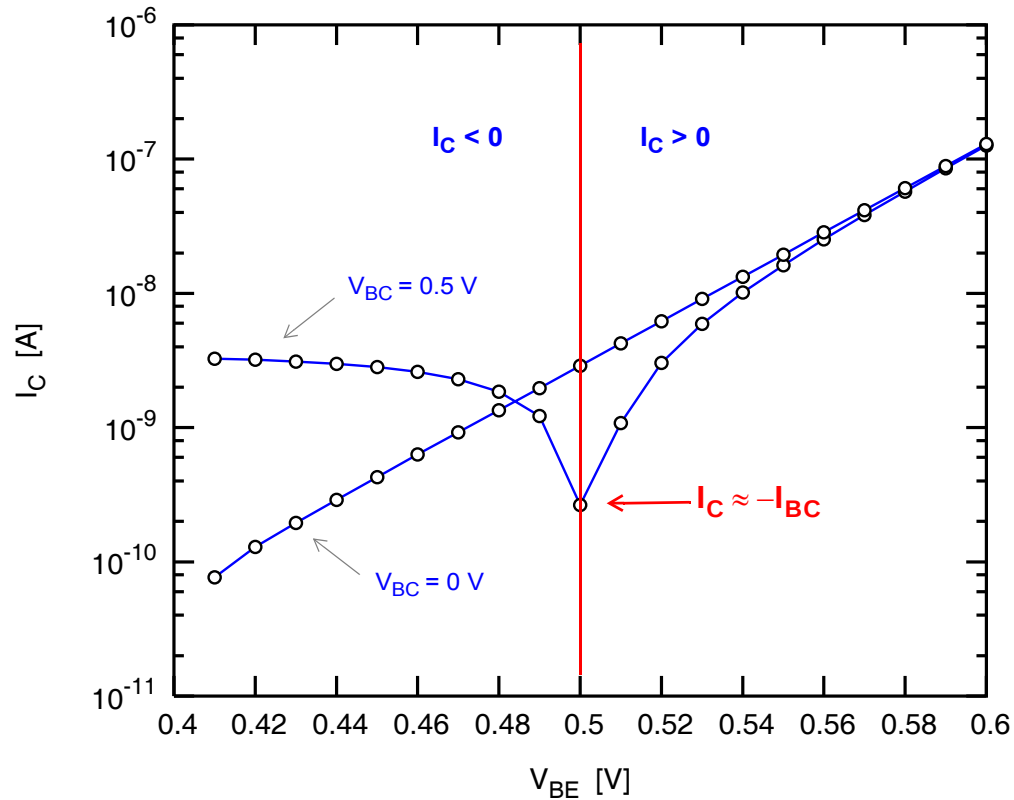


HICUM/L0

- Despite the different approaches used to model the reverse Early effect, all models give similar accuracy (negative slope well described) on the normalized collector current (or current gain), at $V_{BC} = 0 \text{ V}$.
- But it is no more valid for positive V_{BC} , in the saturated region.

1. ST solver

Gummel PLOTS with Positive V_{BC}



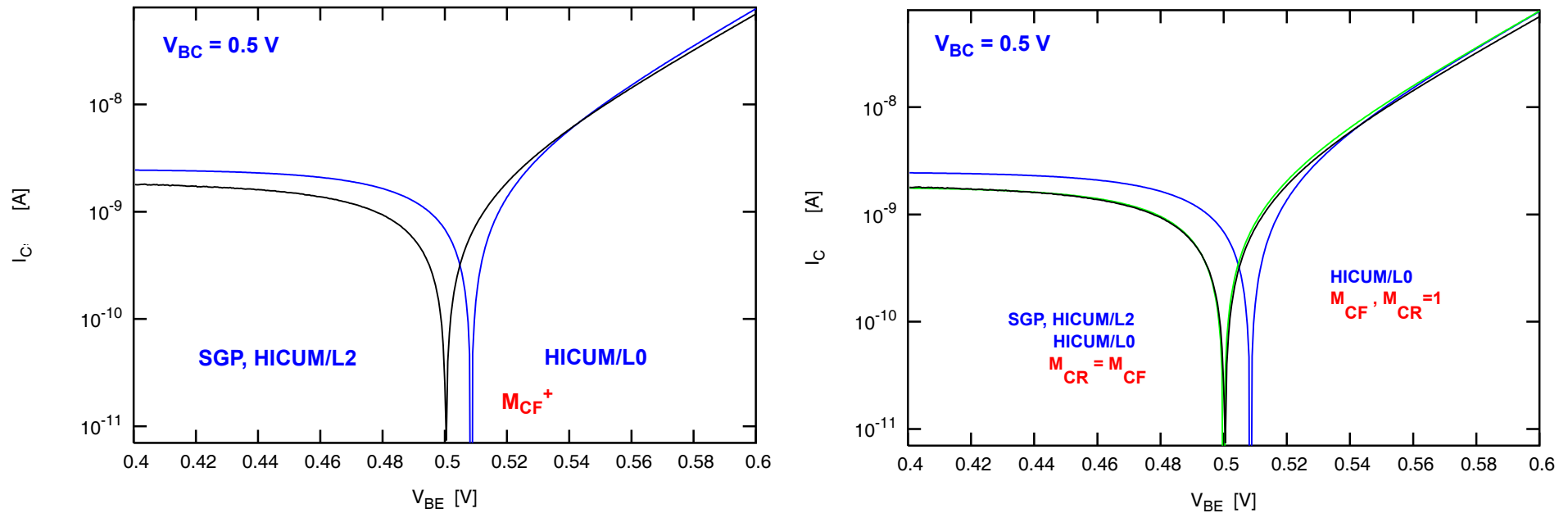
• $I_C = I_T - I_{BC} - I_{SC}$

• at $V_{BC} = V_{BE}$ (0.5 V) $\left\{ \begin{array}{l} I_{SC} \approx 0 \text{ because } V_{sc} = 0 \\ I_T \propto e^{\frac{V_{BE}}{V_T}} - e^{\frac{V_{BC}}{V_T}} = 0 \\ I_C \approx -I_{BC} \end{array} \right.$

but not in HICUM/L0

$$I_T \propto e^{\frac{V_{BE}}{V_T}} - e^{\frac{V_{BC}}{V_T}} \neq 0$$

→ Limitation of HICUM/L0 and solution to minimize this modeling issue

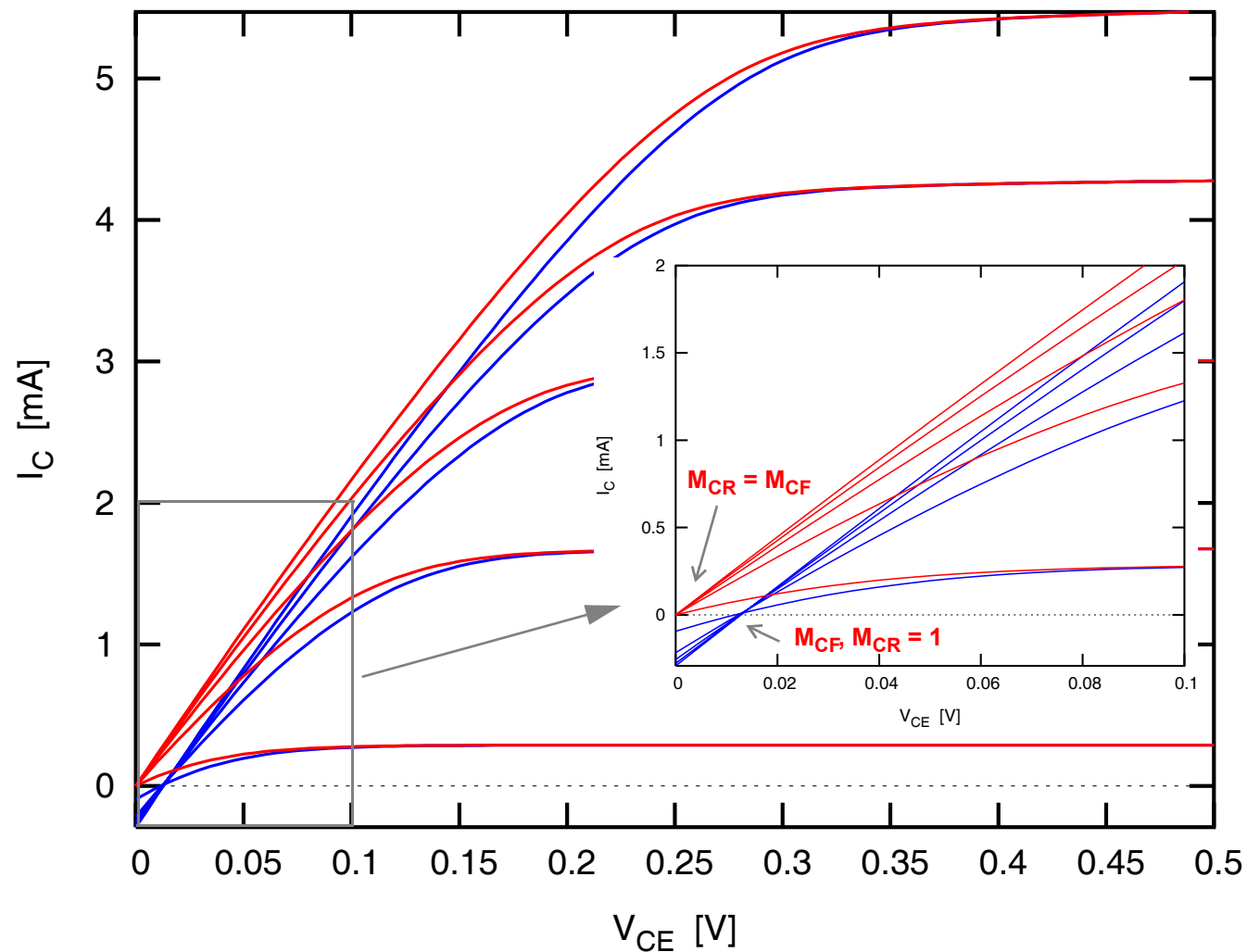


- In saturated region, and especially for $V_{BE} = V_{BC}$, the shift between HICUM/L0 and other models increases with M_{CF} (high reverse Early effect, low reverse Early voltage).
- To minimize this effect, a solution consists of set M_{CR} equal to M_{CF} . Therefore, in this case, the transfer current I_T is equal to zero at $V_{BE} = V_{BC}$

$$I_T \propto e^{\frac{V_{BE}}{M_{CF} \cdot V_T}} - e^{\frac{V_{BC}}{M_{CR} \cdot V_T}} = 0 \quad \text{if } M_{CF} = M_{CR}$$

- This correction is to the detriment of the accuracy on the reverse Gummel plot (slope too low).

- The same behavior can be observed on the forward output characteristics. Here again, M_{CR} needs to be set to M_{CF} in order to fit accurately the characteristics at low V_{CE} .



Summary

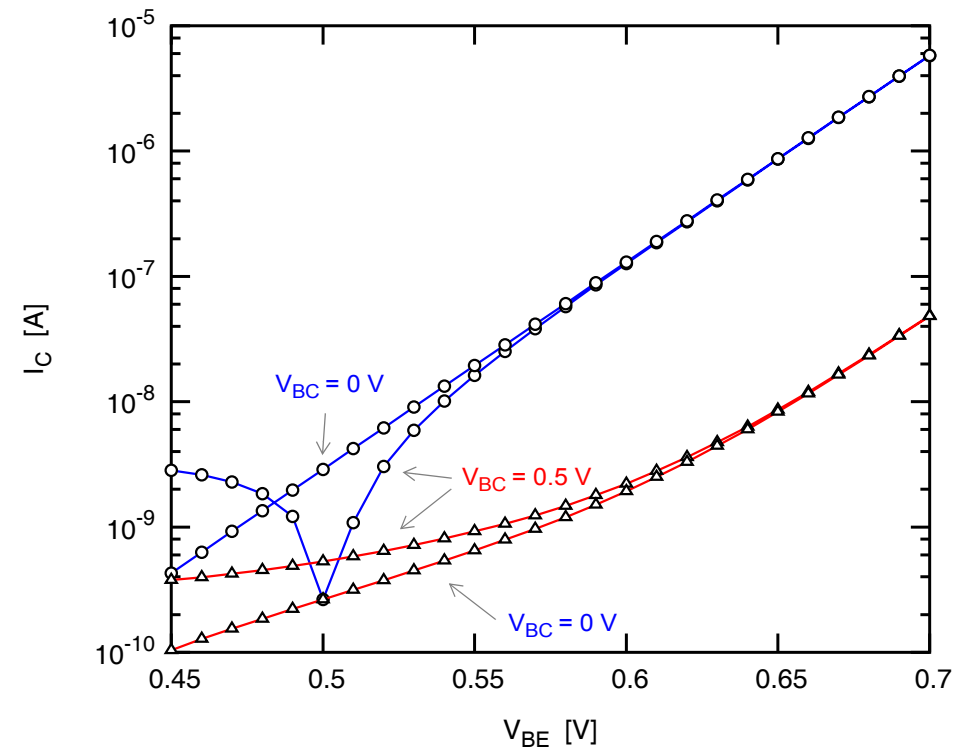
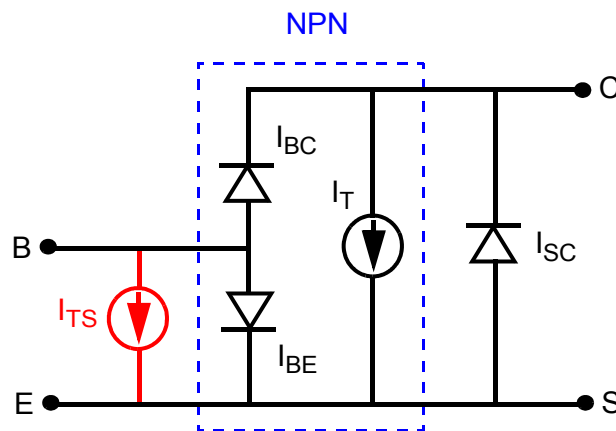
- The modeling of the reverse Early effect in HICUM/L0 has been investigated.
- Its formulation is a simplification of the SPG model which leads to the introduction of a non-ideality factor M_{CF} on the forward transfer current.
- We have demonstrated that in some bias conditions (saturated region), this model can be not enough accurate.
- To overcome this model issue, 2 possibilities:
 - To use the same non-ideality factor in forward and reverse ($M_{CR} = M_{CF}$). Inconsistent with a correct description of the reverse Gummel characteristics.
 - To come back to the SGP model formulation by using a reverse Early voltage V_{AR} instead of a non-ideality factor M_{CF} .
- One pending question: as M_{CF} is linked to V_{AR} via V_T , can we assume M_{CF} temperature independent?

Addenda (1/2)

- An other important limitation of HICUM/L0, in the saturated region, is the lack of parasitic substrate PNP.
- With the present model it is not possible
 - To describe the bias dependence of the forward Gummel plot (especially I_B) with positive V_{BC} .

- $I_C = I_T - I_{BC} - I_{SC}$

- $I_B = I_{TS} + I_{BE} + I_{BC}$



- To accurately model the output characteristics at low V_{CE} .

Addenda (2/2)

- Therefore, the implementation of the parasitic substrate PNP, in HICUM/L0 is always requested (using a flag if needed).

