



Extraction Method for Thermal Resistance

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- Teststructures for temperature measurement
- Example
- Evaluation of recent RTH-extraction method
- Results
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Temperature Measurement

Dependent on the extraction method used different requirements arise:

- DUT and separate sensor
 - some distance from DUT
 - usually requires calibration
 - example : diode
- DUT merged with sensor
 - requires special layout
 - and calibration
 - see example
- DUT as sensor
 - uses regular device
 - best choice

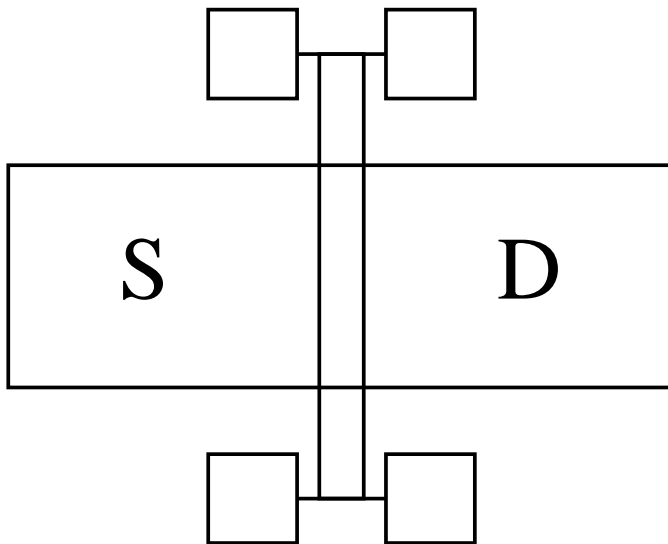


Figure 1: top view of experimental teststructure for temperature measurement

Principle of teststructure for temperature measurement in SOI MOSFET's after [1].

The gate is configured for four-point resistance measurement with calibration in off-state of the MOS.

During operation of the MOS this resistance serves as temperature sensor.

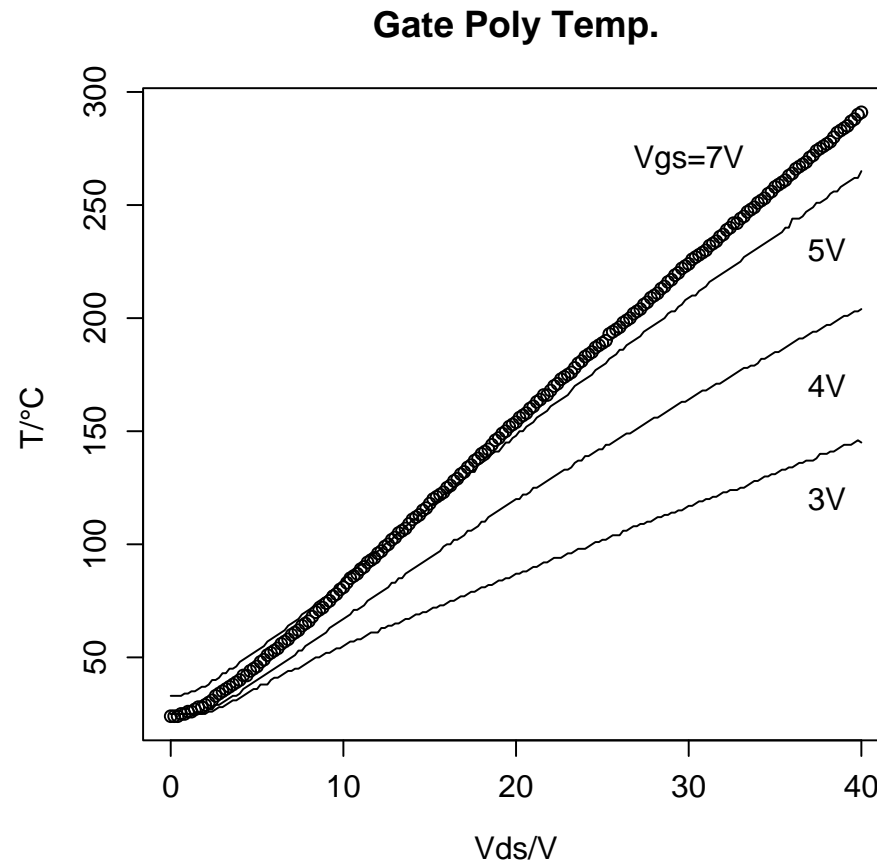


Figure 2: experimental results of SOI NMOS, $w=320\mu m$



RTH-Extraction Method

There are several extraction methods suitable for regular devices [2, 3, 4, 5]. Of particular interest is the method from [5], which allows the extraction of thermal resistance in dependence on ambient temperature.

Thermal conductivity changes with temperature ($\alpha \sim 1.5$) :

$$\kappa(T) = \kappa_{ref} \left(\frac{T}{T_{ref}} \right)^{-\alpha} \quad (1)$$

Since thermal resistance is inversely proportional to the thermal conductivity, we should expect as claimed in [5] :

$$R_{TH}(T) = R_{TH,ref} \left(\frac{T}{T_{ref}} \right)^{\alpha} \quad (2)$$

Total temperature change caused by ambient and power dissipation [4]:

$$\Delta T = R_{TH}(I_C \Delta V_C + \Delta I_C V_C) + \Delta T_A \quad (3)$$

$$\Delta I_C = TC_F(I_C)I_C \Delta T + \frac{\Delta V_C}{V_A} I_C \quad (4)$$

Keeping V_C constant :

$$\Delta T|_{\Delta V_C=0} = R_{TH}V_C \Delta I_C + \Delta T_A \quad (5)$$

$$= \frac{\Delta T_A}{1 - TC_F(I_C)R_{TH}I_C V_C} \quad (6)$$

Keeping T_A constant :

$$\Delta T|_{\Delta T_A=0} = R_{TH}(I_C \Delta V_C + \Delta I_C V_C) \quad (7)$$

$$= \frac{I_C R_{TH} \left(1 + \frac{V_C}{V_A}\right) \Delta V_C}{1 - TC_F(I_C)R_{TH}I_C V_C} \quad (8)$$

Variation of I_C :

$$\Delta I_C = \frac{\partial I_C}{\partial T} \Delta T \quad (9)$$

$$= TC_F(I_C) I_C \Delta T \quad (10)$$

$$= TC_F(I_C) I_C (\Delta T|_{\Delta V_C=0} + \Delta T|_{\Delta T_A=0}) \quad (11)$$

$$= \frac{TC_F(I_C) I_C}{1 - TC_F(I_C) R_{TH} I_C V_C} (\Delta T_A + I_C R_{TH} (1 + \frac{V_C}{V_A}) \Delta V_C) \quad (12)$$

Extraction of R_{TH} :

$$\frac{\frac{\Delta I_C}{\Delta V_C} |_{\Delta T_A=0}}{\frac{\Delta I_C}{\Delta T_A} |_{\Delta V_C=0}} = I_C R_{TH} (1 + \frac{V_C}{V_A}) \quad (13)$$

$$R_{TH} = \frac{I_C(V_C + \Delta V_C, T_A) - I_C(V_C - \Delta V_C, T_A)}{I_C(V_C, T_A + \Delta T_A) - I_C(V_C, T_A - \Delta T_A)} \frac{\Delta T_A}{\Delta V_C} \frac{1}{I_C (1 + \frac{V_C}{V_A})} \quad (14)$$

This is eq. 3 of [5] using I_C instead of I_B as sensed signal.

Measurement conditions :

- DUT : SiGe2_power npn, $4 \times 19.7 \mu m \times 1.3 \mu m$
- $V_C = 2V, \Delta V_C = 0.2V$
- $I_C \sim 1.5mA$ at room temperature
- $\Delta T_A = 10^\circ C$
- change base drive with temperature to keep power dissipation constant

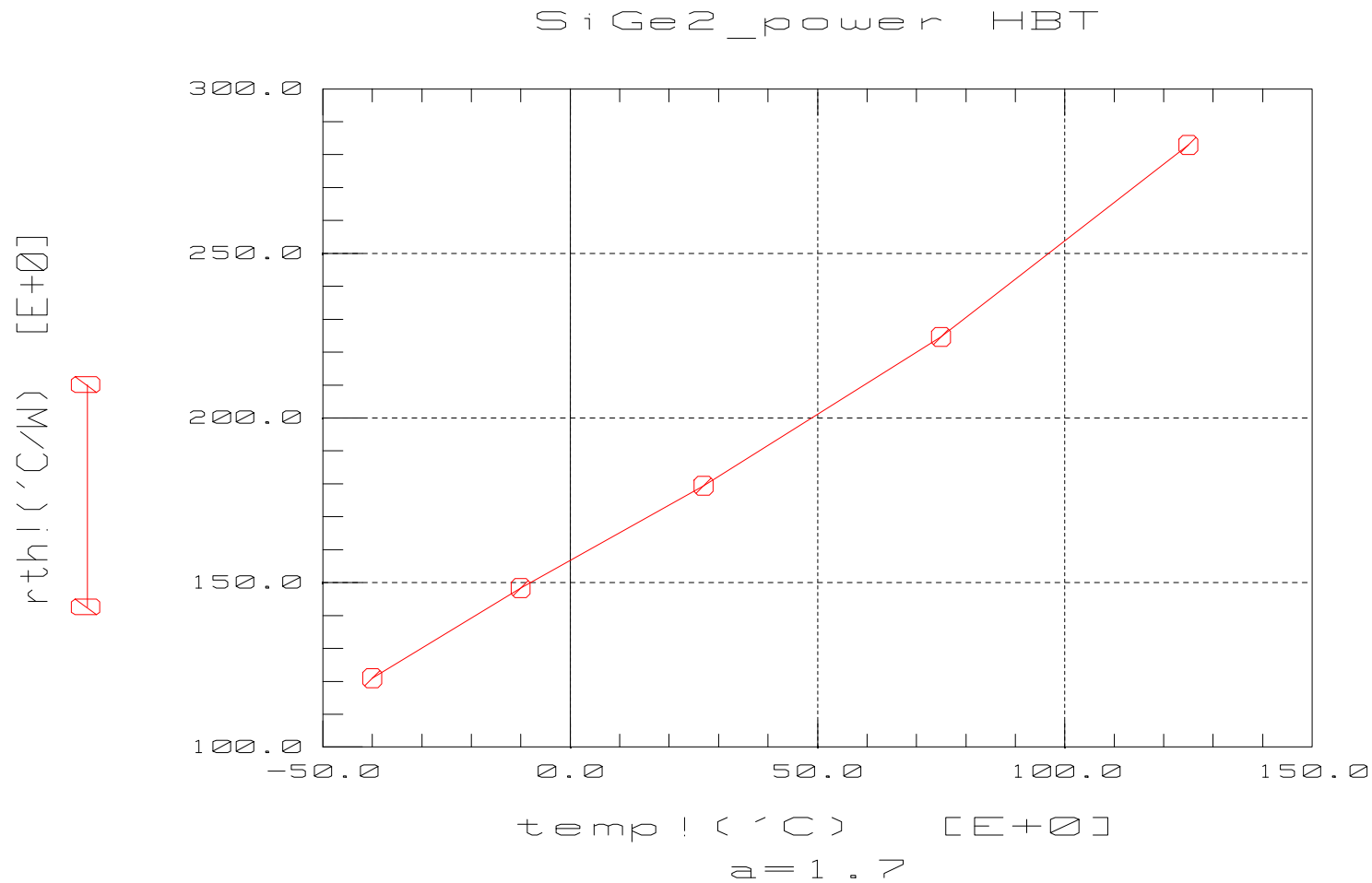


Figure 3: extracted dependence of RTH on ambient temperature

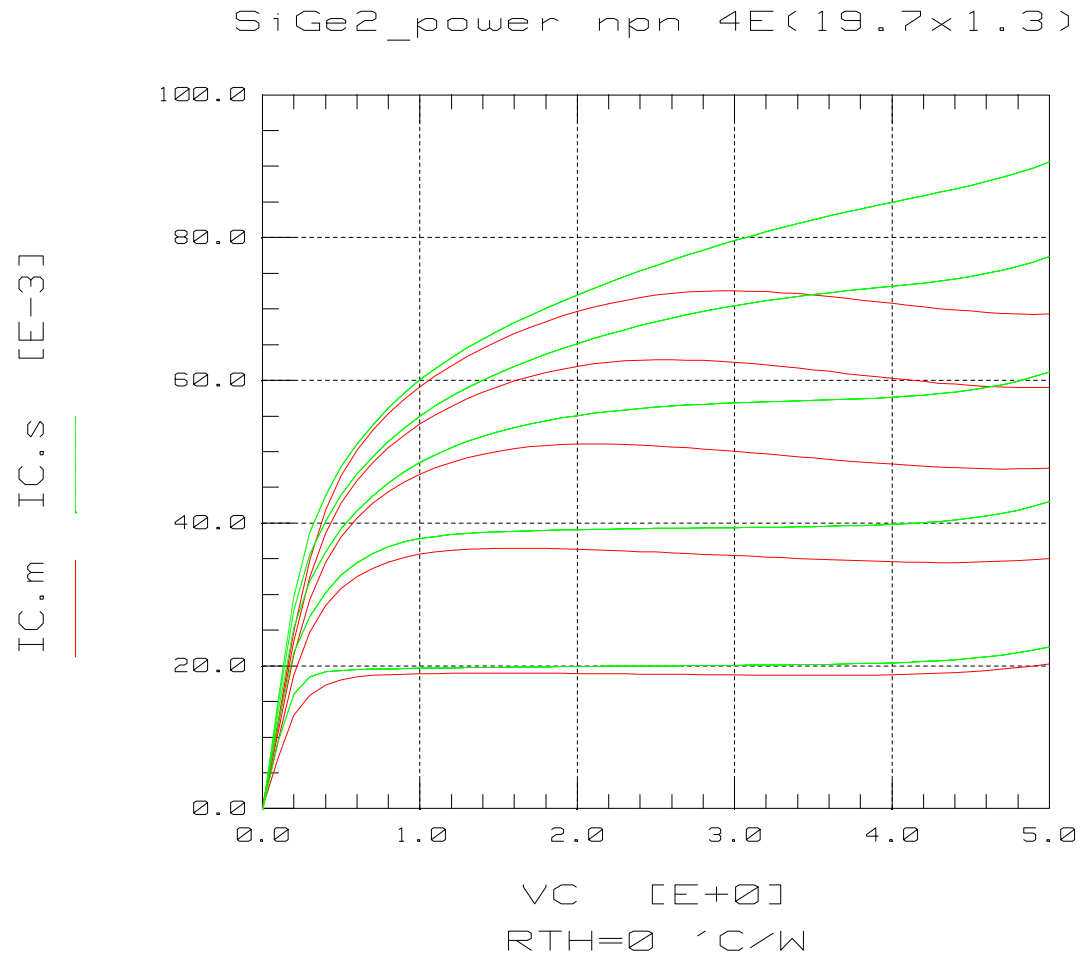


Figure 4: output characteristics of HBT w/o. selfheating

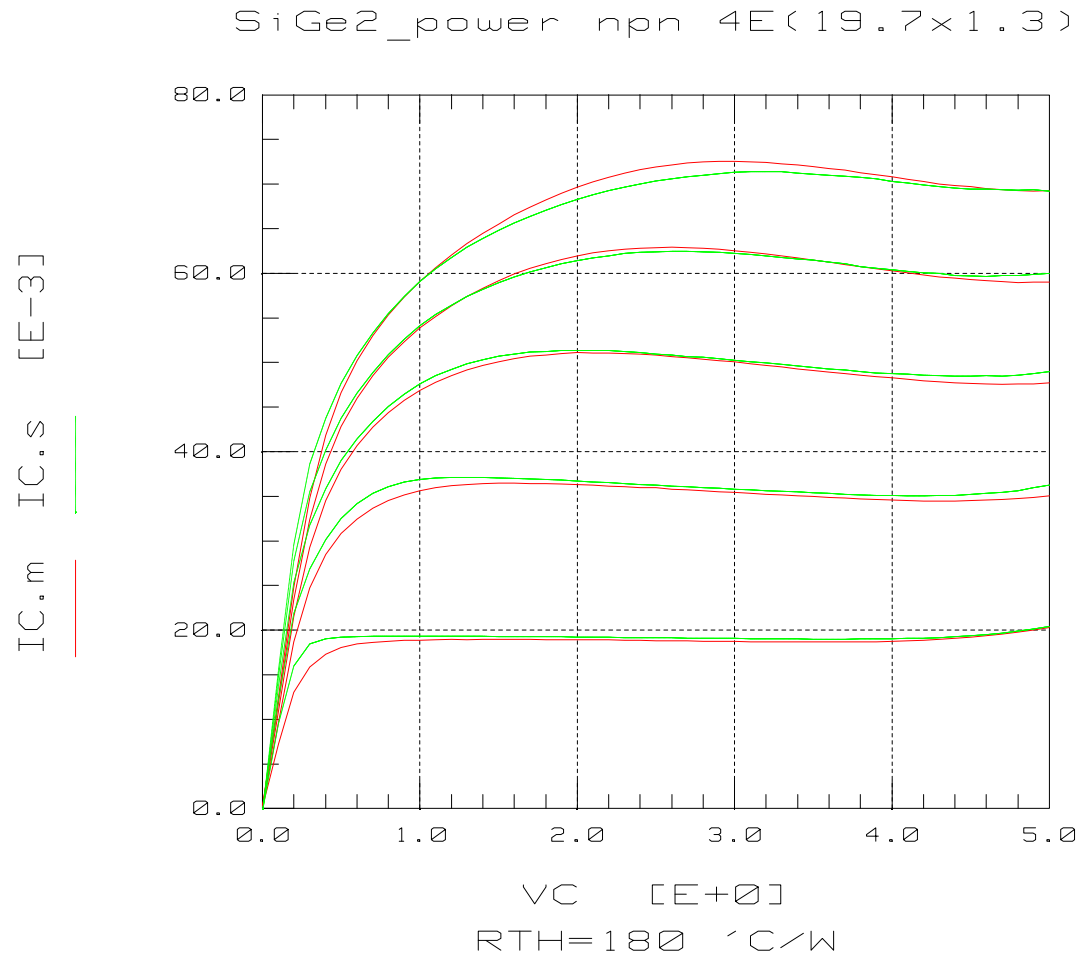


Figure 5: output characteristics of HBT including selfheating

- Most recent method for R_{TH} extraction has been verified
- Thermal resistance depends on temperature
- Therefore selfheating (SH) becomes nonlinear
- Can be handled by Kirchhoff-Transformation [7]
- Models having SH should take that into account

References

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- [4] D.T. Zweidinger *et.al.*, *BCTM*, 1995
- [5] J.C.T. Passchens *et.al.*, *BCTM*, 2004
- [6] M. Reisch ,*Solid-State Electronics*, pp. 677-679, 1992
- [7] K. Poulton *et.al.*, *JSSC*, Oct 1992