

Breakdown mechanisms in advanced SiGe HBTs: scaling and TCAD calibration

T. Rosenbaum^{1,2,3}, D. Céli¹, M. Schröter², C. Maneux³

Bipolar ArbeitsKreis

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¹STMicroelectronics, 38920 Crolles, France

²CEDIC, Technische Universität Dresden, 01062 Dresden, Germany

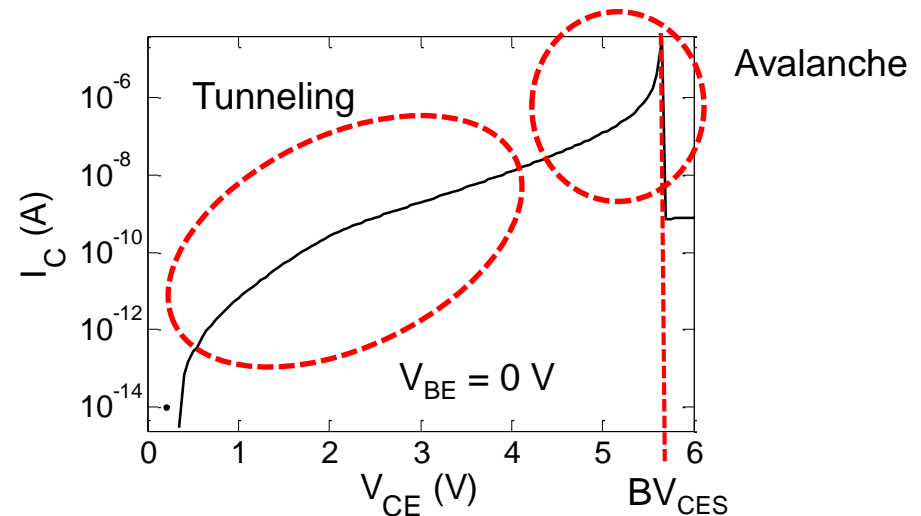
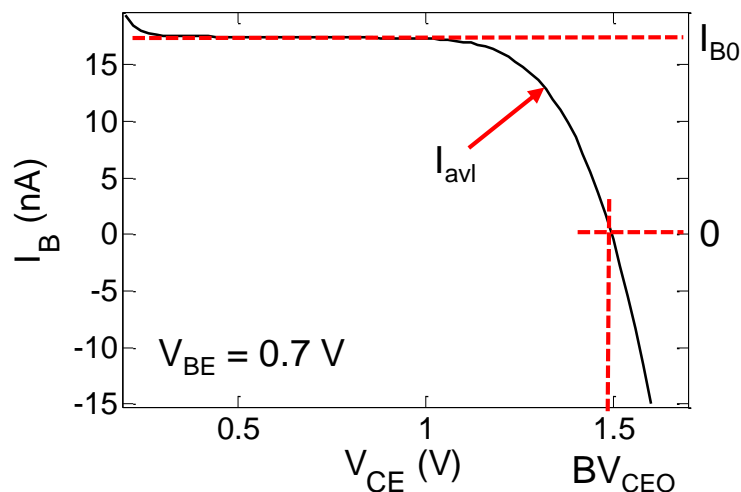
³IMS, Université Bordeaux I, 33405 Talence, France

- Introduction
 - Figures of merit for breakdown characterization
 - P/A scaling and determination of I_{avl} from measurements
- TCAD calibration of impact ionization
 - Calibration of impact ionization parameters
- Tunneling current scaling
 - Well proximity effect
 - Determination of BV_{CES} with TCAD
- Conclusion

- Breakdown voltages

- Are defined for different bias conditions
- BV_{CEO}
 - Sweep V_{CB} until Base current reversal at fixed V_{BE} (e.g. $V_{BE} = 0.7\text{ V}$)
- BV_{CES}
 - Sweep V_{CB} until breakdown of BC diode for $V_{BE} = 0\text{ V}$
- BV_{CBO}
 - Sweep V_{CB} until breakdown of BC diode for floating Emitter contact ($I_E = 0\text{ A}$)

- Examples



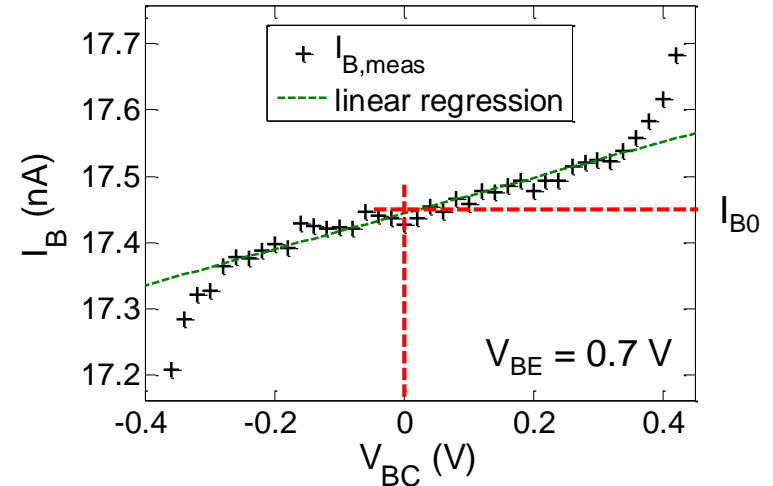
$$I_{avl} = |I_B - I_{B0}|$$

Avalanche current separation

- Zoom-in of Base current of BV_{CEO} measurement

- Zero volt Base current
 - Marks reference point of separation
- Current for positive bias ($V_{BC} > 0.4$ V)
 - Is influenced by injection
- Voltage dependence of current
 - Linear dependence (-0.3 V $< V_{BC} < -0.3$ V)
 - Is caused by neutral base recombination
 - ⇒ taken into account by linear model

$$I_{B,NBR} = I_{B0}(1 + m_{NBR}V_{BC})$$



- Calculation of I_{avl} and I_T

- Linear fit with measurement data to determine m_{NBR}
- Avalanche and transfer current calculation

$$I_{avl} = |I_B - I_{B,NBR}| \quad I_T = I_C - I_{avl}$$

- For TCAD calibration

- Area related components necessary
- ⇒ perform P/A separation

- P/A concept

- Description for total transfer current

$$I_T = J_{TA}A_{E0} + J_{TP}P_{E0}$$

- Current components

- J_{TA} is assumed to be constant over w_{E0}
- J_{TP} is associated with perimeter

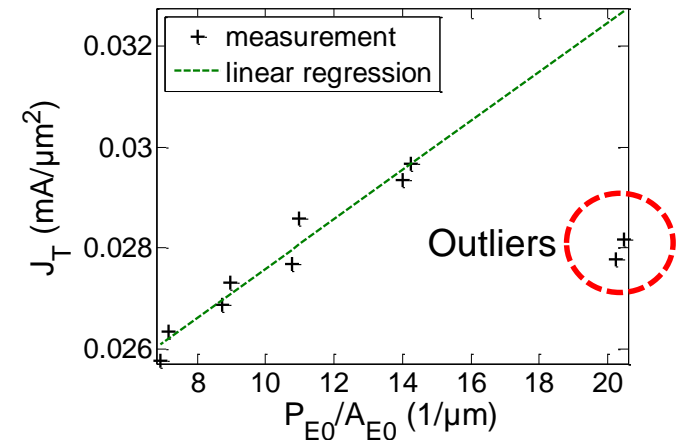
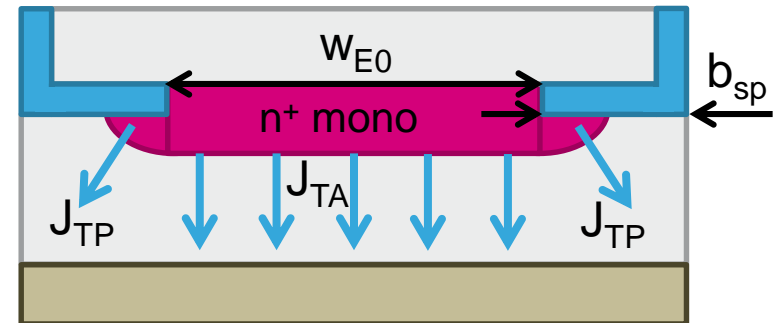
- Example extraction

- Current separation leads to straight line

$$\frac{I_T}{A_{E0}} = J_{TA} + J_{TP} \frac{P_{E0}}{A_{E0}}$$

- Slope of extrapolation corresponds to J_{TP}
- Intercept of extrapolation with $P_{E0}/A_{E0} = 0$ corresponds to J_{TA}

⇒ allows determination of current components for each bias point by linear regression



TCAD reference data

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- Area related avalanche current

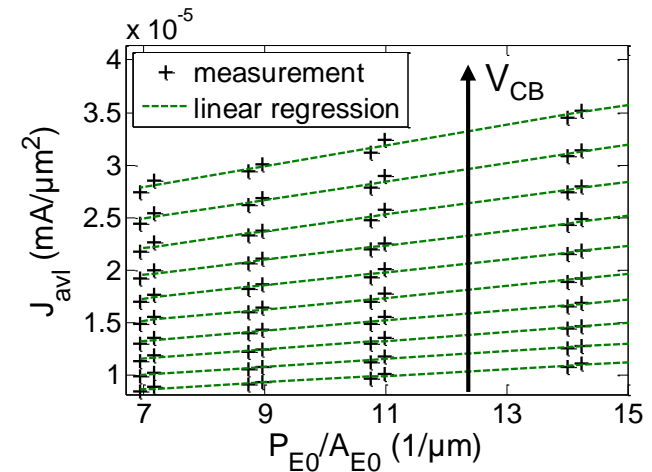
- $J_{av/A}$ is the result of P/A separation of I_{avl}
 - Method applied analog to I_T
- Is $J_{av/A}$ suitable for TCAD calibration?

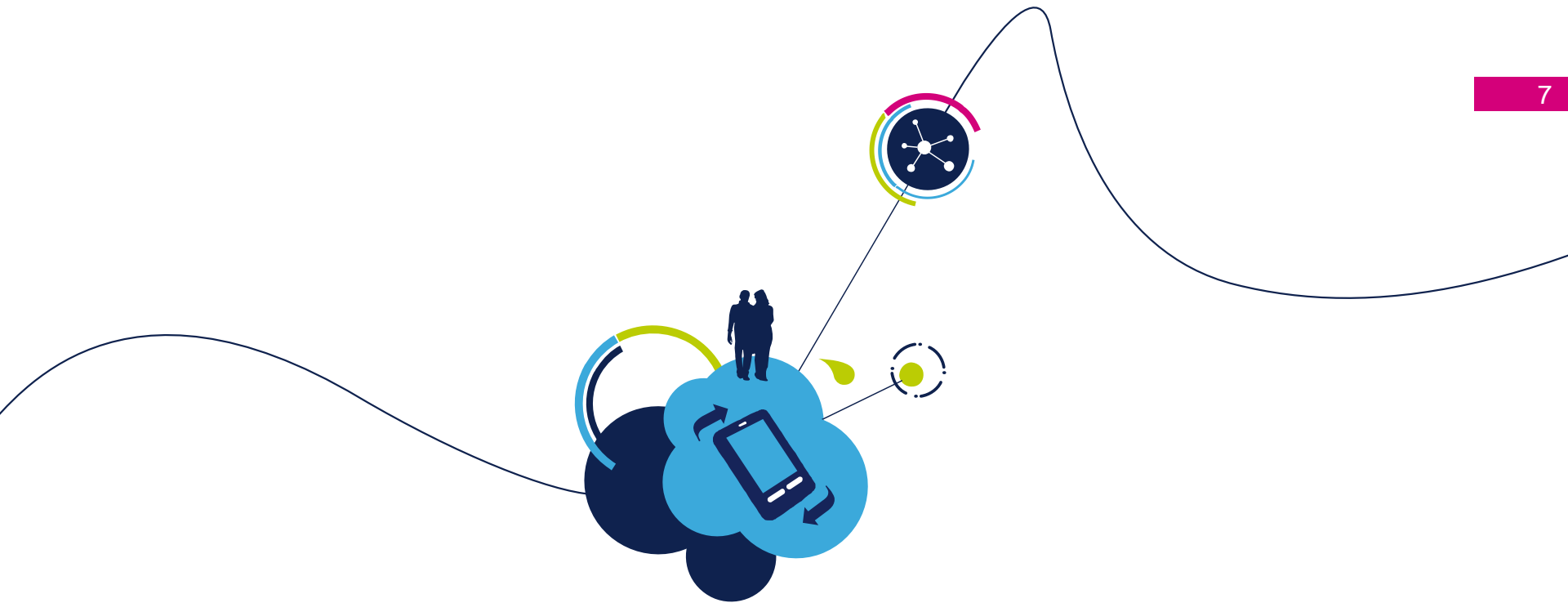
- Physical background of Impact Ionization (II)

- Highly energetic electrons hit electrons in valence band
 - ⇒ bound electrons in valence band can get knocked out of its state causing the generation of electron hole pairs (EHP)
 - ⇒ consecutive collisions lead to avalanche (electrons are **multiplied**)

- Multiplication factor

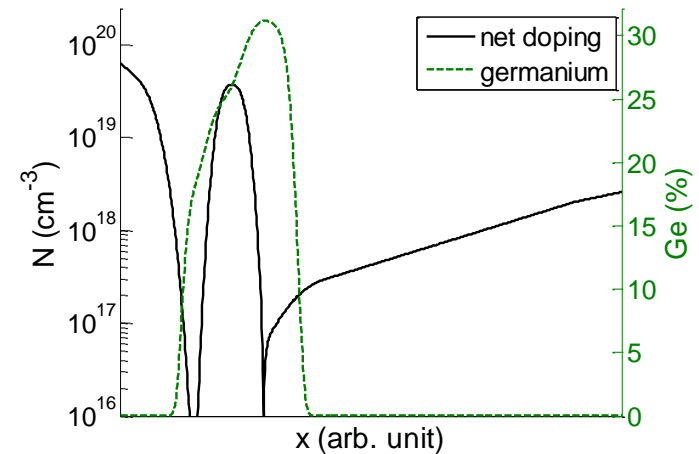
- Definition
$$M = 1 + \frac{I_{avl}}{I_T}$$
- Process of impact ionization is associated to transfer current
 - ⇒ an error of I_T will impact I_{avl}
 - ⇒ use multiplication factor M to calibrate TCAD instead of I_{avl}





TCAD calibration of impact ionization

- Calibrated 1D doping profile
 - See reference [1]
- TCAD environment
 - In-house HD simulator of TU-Dresden with 1D simulation capability



- Avalanche model for electrons (HD)
 - Generation rate is associated to carrier temperature

$$G_{avl,n} = nA \exp\left(-B \frac{E_G}{k_B T_n}\right)$$

- Model parameters A and B are to be calibrated
- Adjustment procedure
 - Run optimization on A and B for best agreement with measurement data

Parameter adjustment

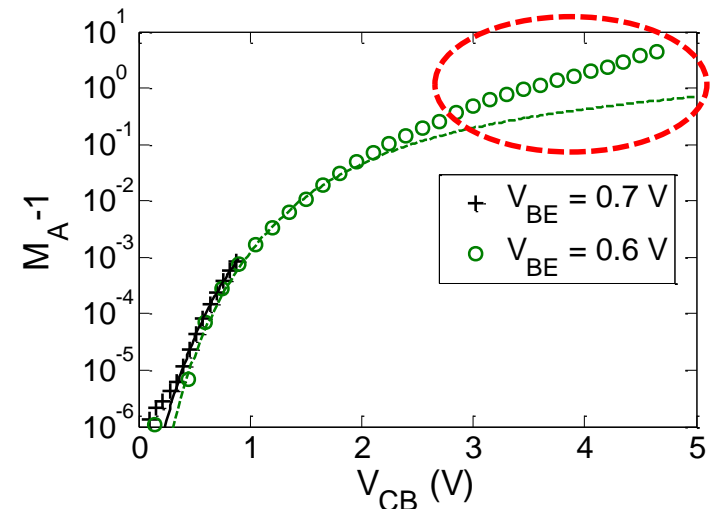
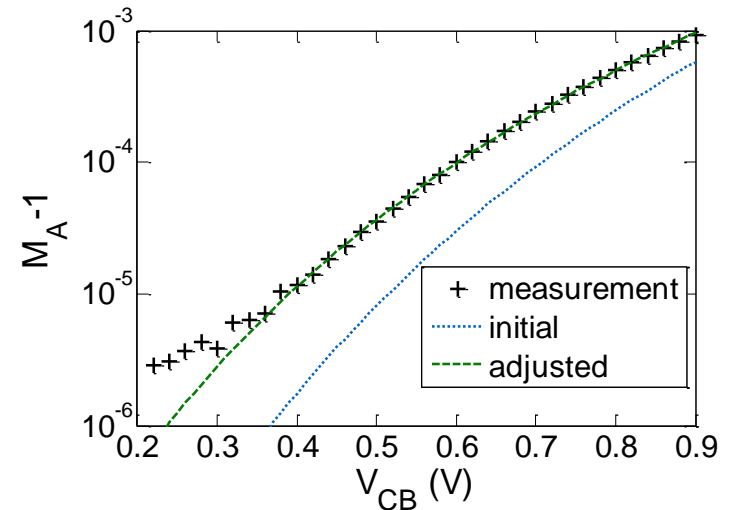
- Comparison

- M_A denotes multiplication factor of area component
- Initial parameters
 - $A = 2.514e+015$ 1/s, $B = 4.869$
- Adjusted parameters for best fit
 - $A = 1.770e+014$ 1/s, $B = 3.668$

⇒ very good agreement for analyzed bias range

- Extended bias range

- Forced V_{BE} measurement available up to $V_{CB} = 5$ V (single transistor data only)
 - $V_{BE} = 0.6$ V
 - Need to assume identical scaling to obtain M_A
- Good agreement with measurement data up to $V_{CB} = 2$ V
 - Markers correspond to meas
 - Lines correspond to simulation
- Deviation for $V_{CB} > 3$ V ?

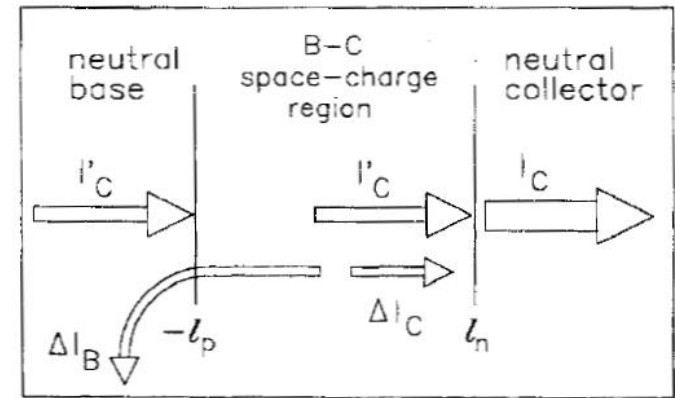
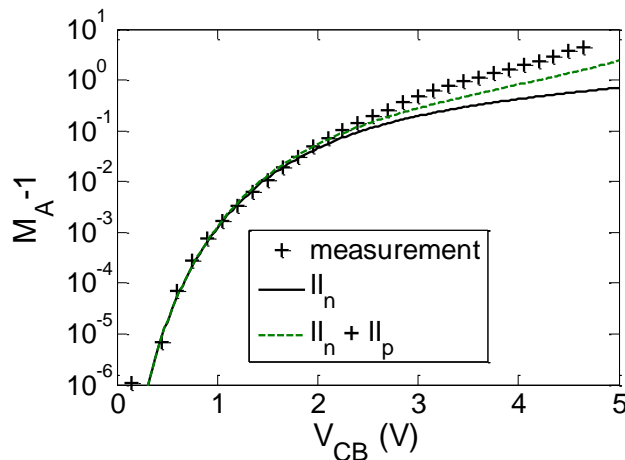


Including impact ionization of holes

- Electron hole pair (EHP) generation
 - Can also be triggered by holes
 - Is the process relevant for npn transistors?
 - At low electric fields the EHP generated by holes is negligible as the amount of holes is small
 - For large electric fields holes of EHP generated by electrons can cause an avalanche

• Simulation rerun improves result

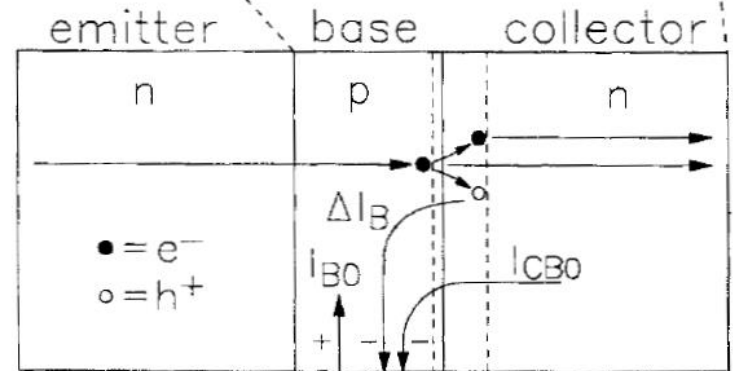
- Avalanche for holes activated
 - Using standard parameters



$$I_C = M I'_C = I'_C + |\Delta I_B|$$

$$= I'_C + \Delta I_C$$

[2]



[2] C. Canali et al., "Experimental and Monte Carlo analysis of impact-ionization in AlGaAs/GaAs HBTs", IEEE Transaction on Electron Devices, 1996.

Final calibration result

- Final steps for calibration of avalanche parameters
 1. Adjust hole parameters for extended measurement range
 2. Check agreement for standard range and re-adjust parameters for electrons
 3. Loop for best fit
 - For holes, DD transport is assumed => different II description
- Avalanche model for holes (DD)

$$G_{avl,p} = p v_{sp} a_p \exp\left(-\frac{F_p}{grad[\varphi_p]}\right)$$

- Comparison

- Initial parameters

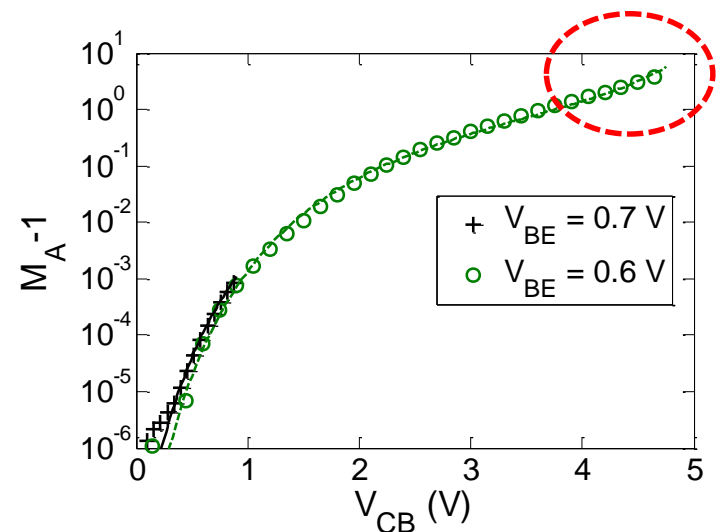
- $A = 2.514e+15$ 1/s, $B = 4.869$
 $a_p = 1.582e+06$ 1/cm, $F_p = 2.036e+06$ V/cm

- Adjusted parameters for best fit

- $A = 1.250e+14$ 1/s, $B = 3.552$
 $a_p = 1.3213e+06$ 1/cm, $F_p = 1.2938e+06$ V/cm

⇒ good agreement for whole bias range

- Both $V_{BE} = 0.6$ and $V_{BE} = 0.7$ V are captured reasonably well
 - Onset of breakdown is captured (see red circle)



BV_{CEO} vs. B_f comparison

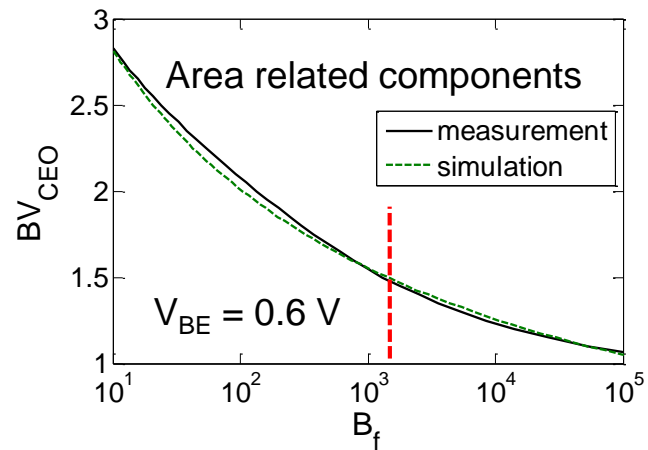
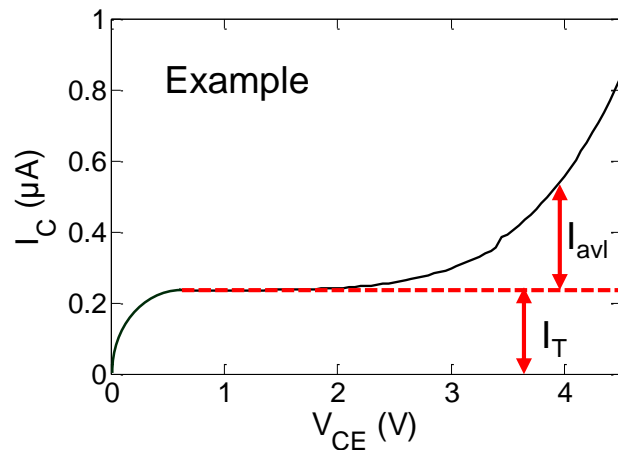
- TCAD limits

- Base current is usually insufficiently accurate
 - Caused by recombination component of E contact and maturity of the process
- ⇒ typically, I_B cannot be determined reliably from TCAD simulations
- ⇒ workaround for BV_{CEO} required

- Plot breakdown voltage vs. current gain

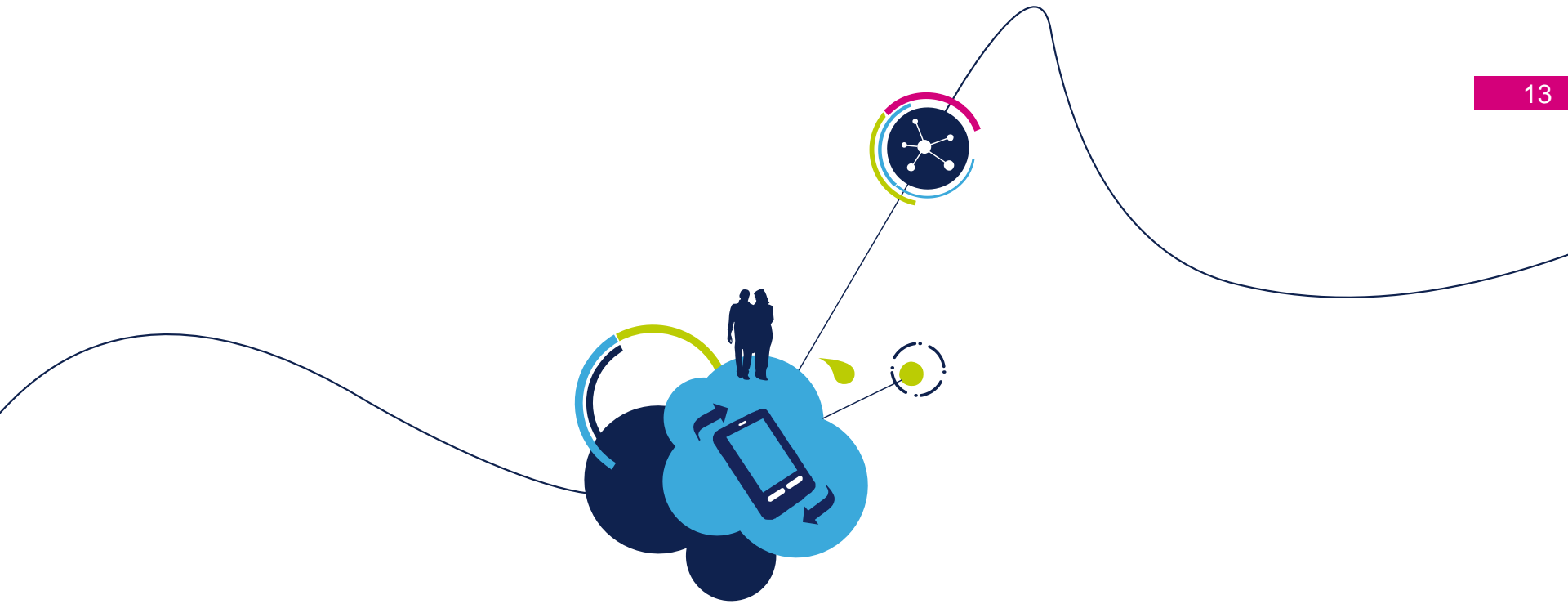
- Assuming breakdown at an arbitrary V_{CE}
 - I_{avl} must be as large as I_B at breakdown condition
 - ⇒ calculate B_f from I_{avl} and I_T

$$\frac{I_T}{I_{avl}} \Big|_{BV_{CEO}} = \frac{I_B B_f}{I_B} = B_f$$



- Good agreement with measurement data

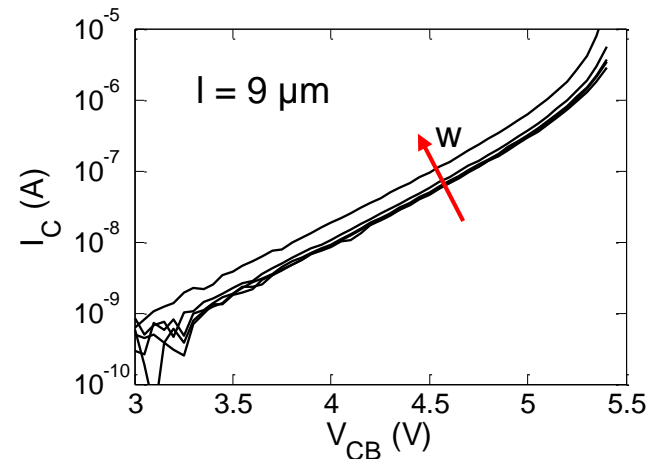
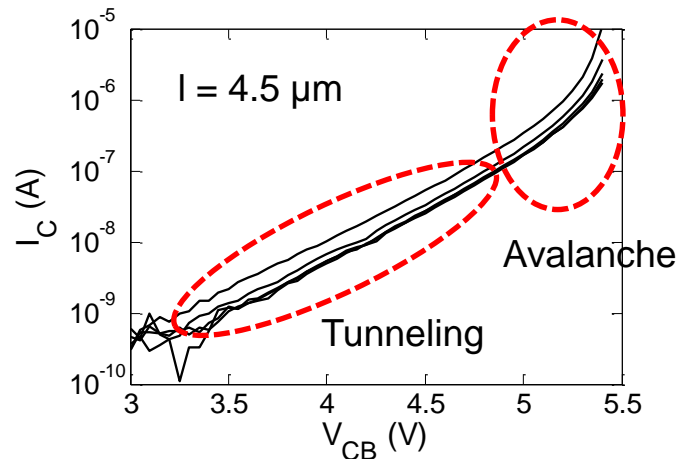
- BV_{CEO} = 1.49 V (sim) vs. 1.48 V (meas)



Tunneling current scaling

- Measurement data overview

- $V_{BE} = 0$ V, V_{CB} sweep until breakdown
 - BE diode deactivated, BC diode in reverse operation
 - Leads to tunneling and avalanche current of BC diode



- Unexpected device behavior
 - Increasing current with decreasing width, or (if excluding smallest width) no dependence of I_C with Emitter width
- Tunneling current
 - Seems to be associated with transistor periphery
 - Increased Collector doping at periphery?

Well proximity effect

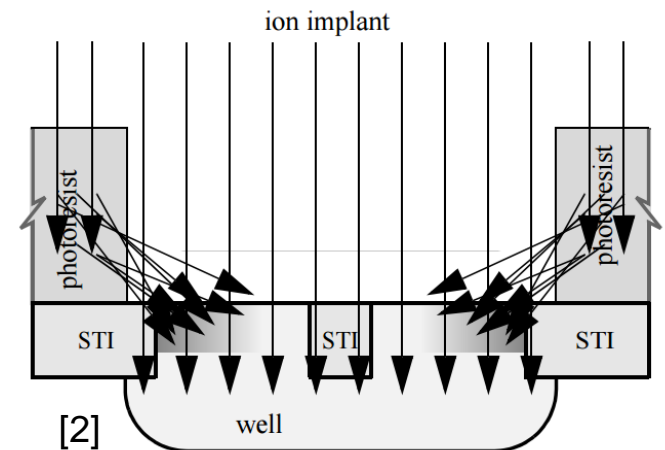
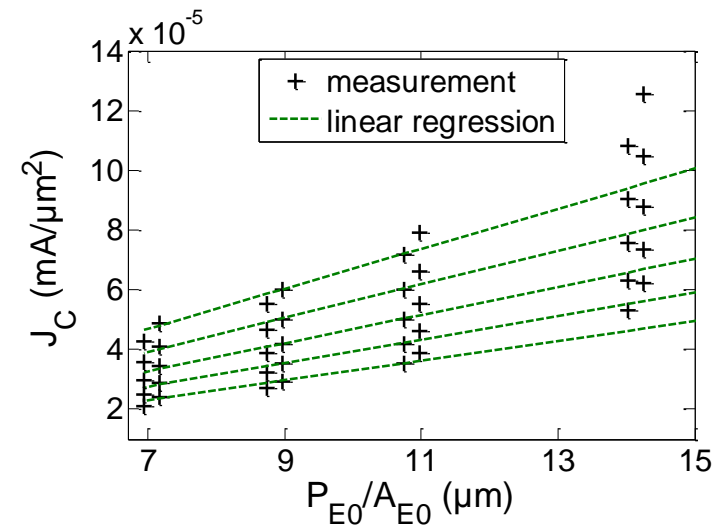
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- Linear regression on measurement data

- Leads to negligible area component I_{tunA}
 - Smallest transistor widths excluded from fit
- ⇒ tunneling current is a perimeter associated phenomenon
- ⇒ indicator for increased Collector doping at periphery

- Well proximity effect (WPE)

- Name originates from well implant of CMOS processes
 - Implant is used to protect devices from latch-up effect
- Implanted ions scatter from photoresist
 - Ions are embedded at lateral photoresist boundary
 - Ions contribute to peripheral doping profile
- For SiGe HBTs, the WPE affects the SIC implant
 - ⇒ ions are attached to Collector periphery



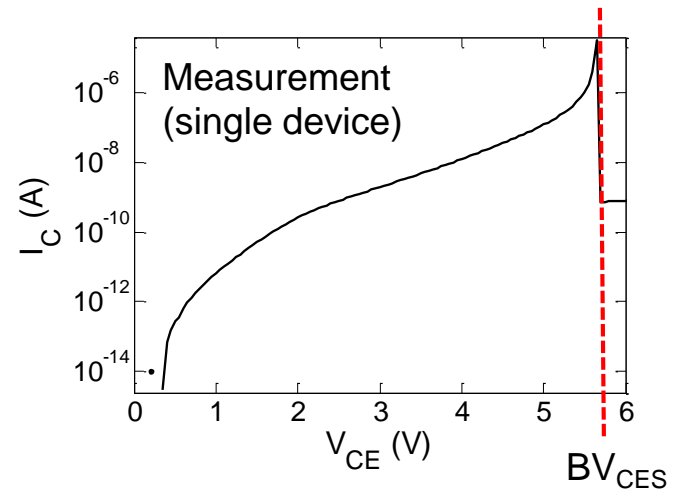
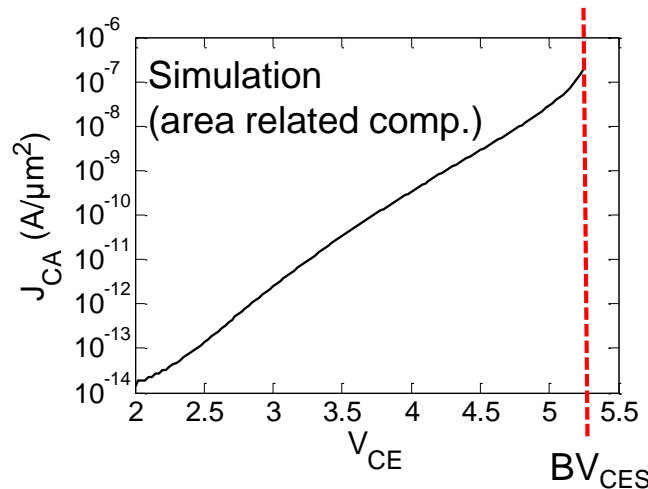
Calibration of tunneling parameters

- Feasibility

- Used process does not exhibit an area related tunneling component
 - Peripheral doping profiles are not known accurately
 - Process-TCAD does not take into account the WPE
- ⇒ calibration of tunneling is **not feasible**

- Assuming standard parameters for tunneling mechanisms

- Avalanche, trap-assisted tunneling (TAT) and band-to-band (B2B) tunneling taken into account for simulations



- Similar breakdown voltages

- 5.3 V (sim.) vs. 5.7 V (meas.)
- But: tunneling current cannot be compared (single transistor vs. area component)

- Tunneling current parameter influence

- Parameters determine shape of $I_C(V_{CE})$ curve ($V_{BE} = 0$ V)
 - But at breakdown condition: carrier impacts multiply infinitely
- ⇒ tunneling parameters should not play a major role, as already a small amount of carriers will trigger breakdown

- Band to band tunneling model

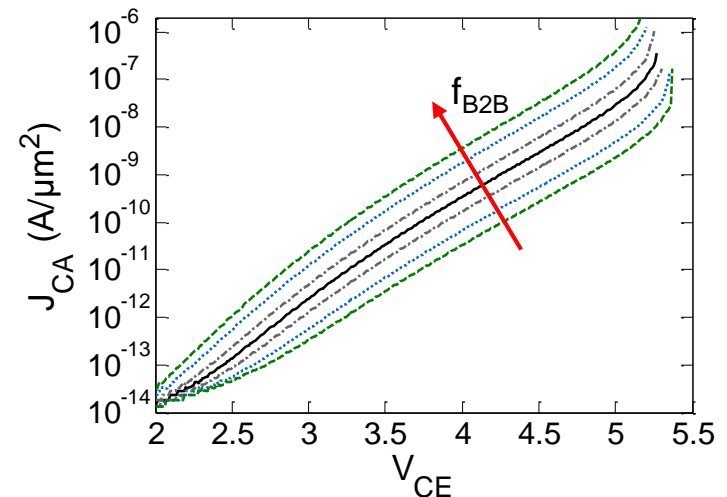
- Field dependent description
 - Parameters f_{B2B} , γ_{B2B} and b_{B2B}

$$G_{B2B} = -f_{B2B} \frac{|F|^{\gamma_{B2B}}}{\sqrt{V_g}} \exp\left(-b_{B2B} \frac{V_g^{3/2}}{|F|}\right)$$

- TCAD analysis

- f_{B2B} variation (span of 2 decades)
 - Minimum value: 3.5e20
 - Reference value: 3.5e21
 - Maximum value: 3.5e22
- BV_{CES} variation
 - 5.20 V ... 5.37 V

⇒ variation relatively small, but standard parameter set should be taken into account



- Introduction on breakdown of SiGe HBTs
 - Physical mechanisms
 - Impact ionization, tunneling
 - Corresponding figures of merit
 - BV_{CEO} , BV_{CES}
- TCAD calibration of an advanced SiGe HBT technology [4]
 - P/A separation of measurement data
 - Calibration of impact ionization parameters
 - Both holes and electron parameters adjusted to measurements
 - Suitability for future doping profiles yet to be verified
- Tunneling current scaling
 - Well proximity effect
 - Determination of BV_{CES} with TCAD successful
 - Sensitivity analysis of tunneling on BV_{CES}

[4] P. Chevalier et al. « A 55 nm Triple Gate Oxide 9 Metal Layers SiGe BiCMOS Technology Featuring 320 GHz fT / 370 GHz f_{MAX} HBT and High-Q Millimeter-Wave Passives ». Proc. IEEE IEDM, 2014.

- [1] T. Rosenbaum et al., “Calibration of 1D Doping Profiles of SiGe HBTs”, accepted paper for Proc. IEEE BCTM, 2015.
- [2] C. Canali et al., “Experimental and Monte Carlo analysis of impact-ionization in AlGaAs/GaAs HBTs”, IEEE Transaction on Electron Devices, 1996.
- [3] P. G. Drennan et al., “Implications of Proximity Effects for Analog Design”, IEEE 2006 Custom Integrated Circuits Conference, 2006.
- [4] P. Chevalier et al. « A 55 nm Triple Gate Oxide 9 Metal Layers SiGe BiCMOS Technology Featuring 320 GHz f_T / 370 GHz f_{MAX} HBT and High-Q Millimeter-Wave Passives ». Proc. IEEE IEDM, 2014.

Thank you for your attention!