

Characterization and modeling of thermal impedance for advanced SiGe HBT

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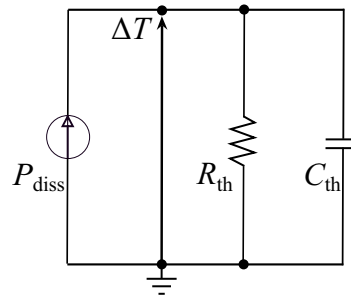
Outline

1. Introduction
2. Measurement and characterization of Y-par and Z_{th}
3. Extraction method for Z_{th}
4. Different thermal networks versus measurements
5. Characterization of T dependence of thermal impedance
6. Summary

Introduction

Introduction

- Mainstream HBT/BJT compact models utilize single-pole thermal network
 - good accuracy at high frequency above 1 GHz;
 - computation efficient due to two elements.

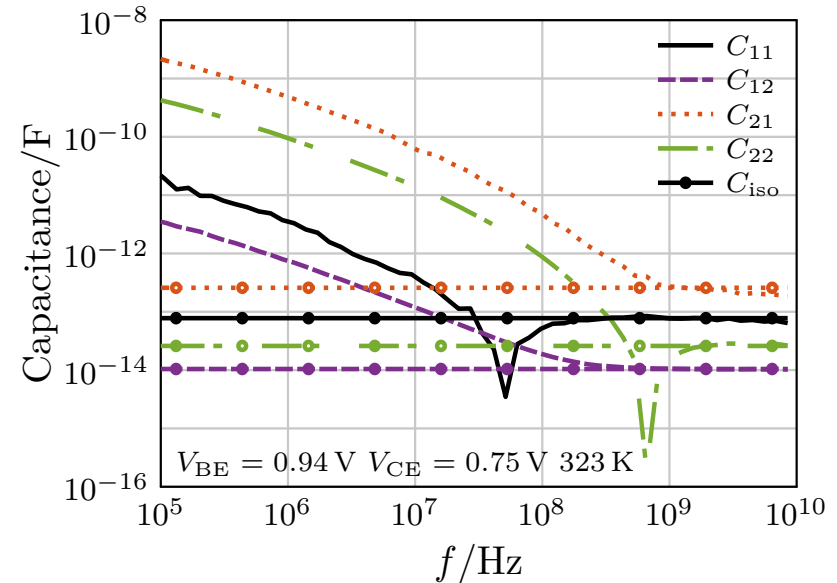
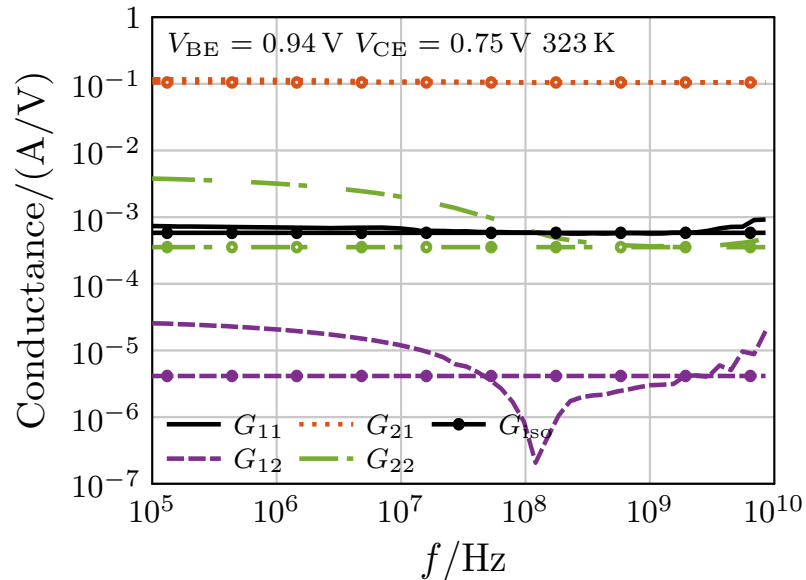


single-pole network

- Measurement, characterization, and multi-pole thermal network modeling have been done for many BiCMOS technologies (DTI/STI) but SG13G2
=> here focus on SG13G2 (only has STI)
- Modeling purpose:
 - intermediate frequency circuits below 1 GHz with large power consumption => AC SH is relevant.
- Investigation on the extraction method for SG13G2

Conductance and capacitance parameter

real(Y) imag(Y/(2*π*f))



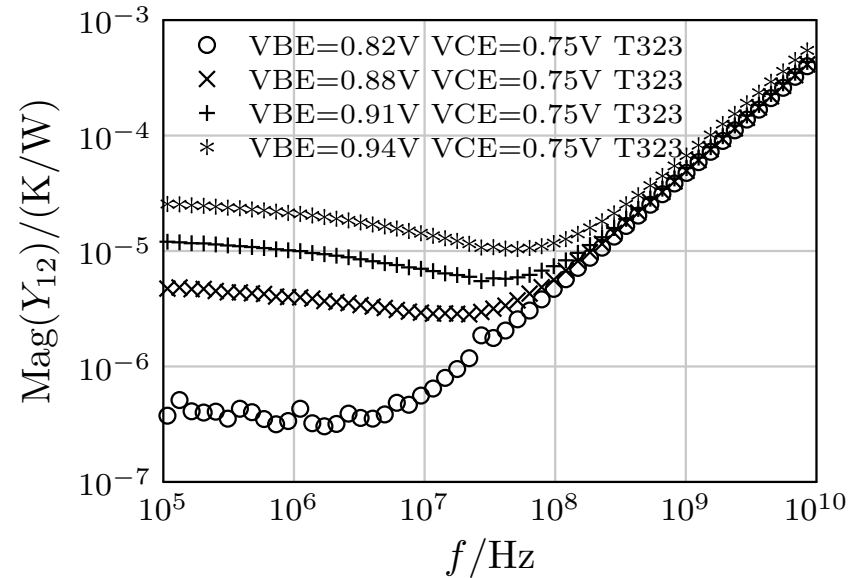
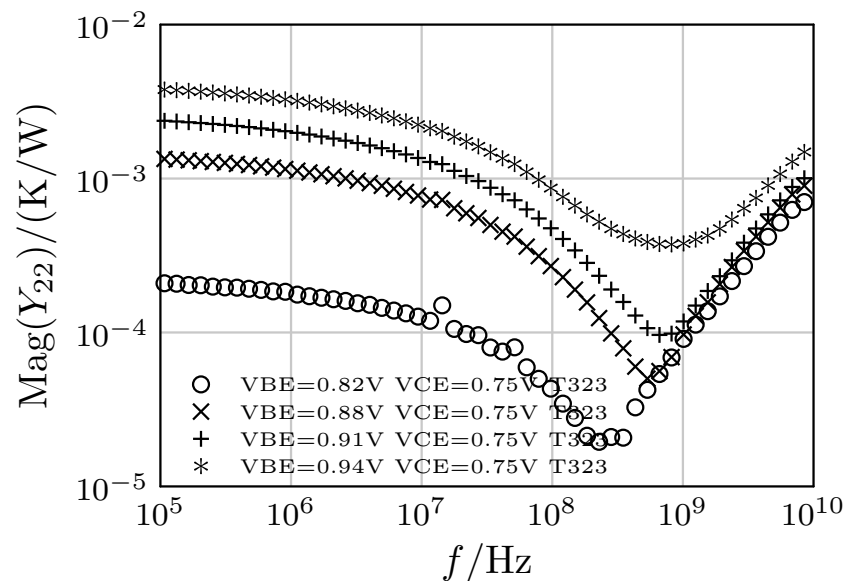
- G(G22 and G12) parameters (real(Y)) and C parameters (imag(Y/(2πfreq))) decreases with frequency;
- SH
 - Below 1 GHz: AC+DC SH readout circuit for quantum computing;
 - above 1 GHz: only DC SH -- most SiGe HBT based circuits;
- Y22 and Y12 are more sensitive to SH, and used as reference to characterize thermal impedance and verify thermal network
 - All C parameters change a lot with frequency;
 - G11 and G21 changes slightly with frequency, whereas G22 and G12 change a lot with frequency;

Measurement and Characterization

Measurement setup

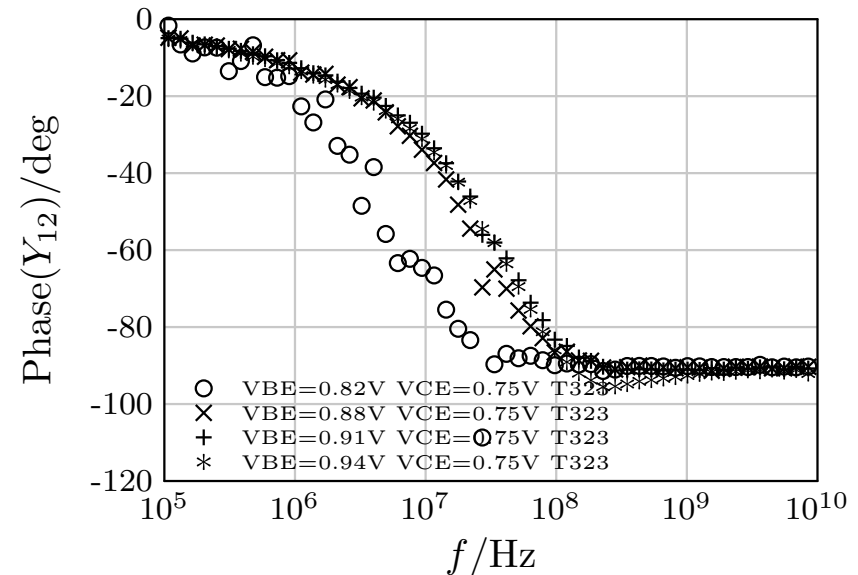
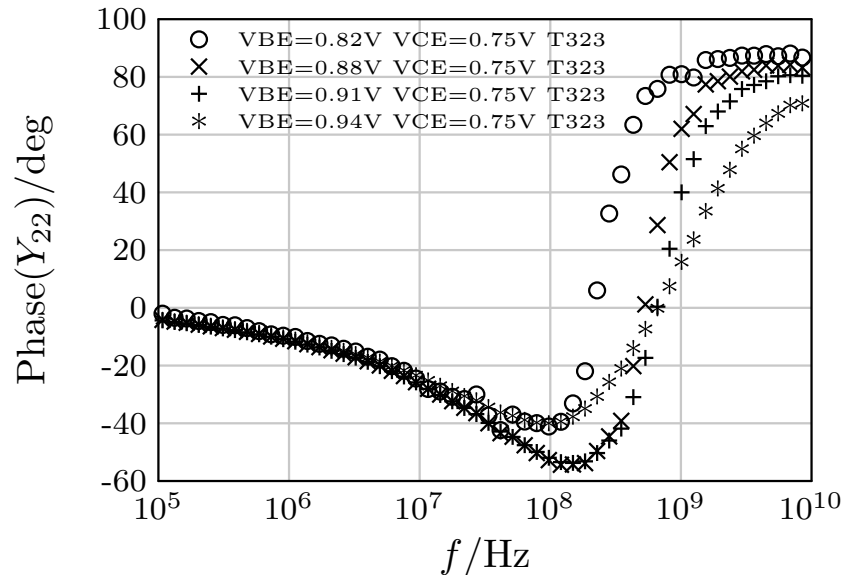
- Technology: SG13G2
- Device: $b_{E0} = 0.12 \mu\text{m}$, $l_{E0} = 0.95 \mu\text{m}$ in CEB configuration, $N_x=4$
- DC: HP 4142B Modular DC Source/Monitor
- S-Parameters: Rohde&Schwarz ZNB8 for 9 KHz-8.5 GHz
- Probe: FormFactor C1N |Z| probes from DC-67 GHz
- Probe station: Süss MicroTec PA 200
- Measurement script: pylab (Christoph Weimer)

Magnitude of Y22 and Y12



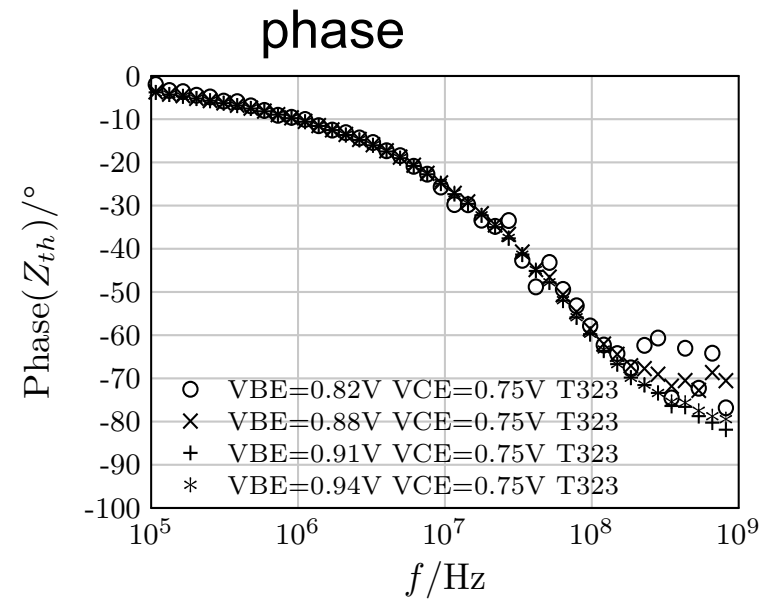
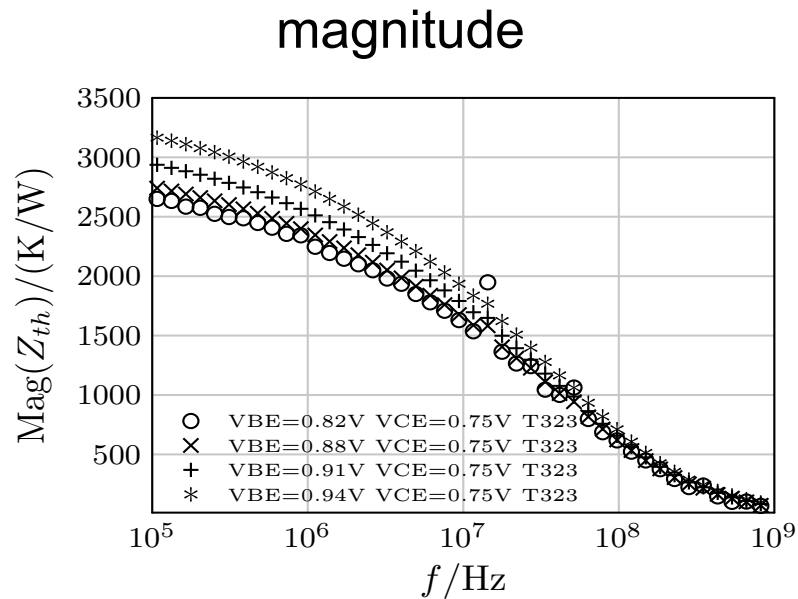
- Y22 and Y12 are more sensitive to SH;
- Increased $\text{mag}(Y_{22})$ and $\text{mag}(Y_{12})$ with V_{BE} due to bias dependence of diode and transfer current;
- Slight reduction of magnitude with frequency at lower frequency range;
- Magnitude decreases smooth with frequency
 => may indicate a relatively **uniform distribution of thermal conductivity**
 => the STI does not located in the heat path.
- **nonuniform => may have the kink in the curve.**

Phase of Y22 and Y12



- Decrease of phase (from 0) starts slightly below 0.1 MHz => AC SH starts to disappear;
- Sign change of phase(Y22) between 100 MHz and 1 GHz due to the sign change of $\text{imag}(Y22)$;
- Constant values of phase(Y22)(= 90°) and phase(Y12)(= -90°) at high frequency indicate that imaginary part is much larger than real part with increased frequency for Y22 and Y12.

Thermal impedance



- Mag(Z_{th}) and Phase(Z_{th}) decrease with frequency from 0.1 MHz to around 1 GHz:
 - AC SH disappears with increased frequency;
 - Maximal phase reached is around 80°.
- Mag(Z_{th}) increases with V_{BE} for same V_{CE} due to the increase of I_C causing high $T_{junction}$.
- Monotonous reduction of Z_{th} without kink may demonstrate the uniform heat diffusion.

Extraction method

Z_{th} extraction method

- y parameter method:

$$Z_{th} = \frac{y_{22} - y_{22T}}{c_m (I_C + V_{CE}y_{22} + V_{BE}y_{12})(1 + b)}$$

- y_{22T} is the isothermal y_{22} , i.e., where AC SH disappears;
- c_m is given by

$$c_m = \frac{\partial I_C}{\partial T},$$

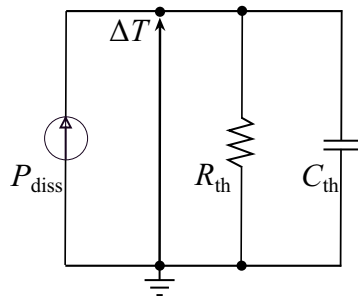
- b is given by

$$b = \frac{P}{Z_{th}} \frac{\partial Z_{th}}{\partial P} \Big|_T$$

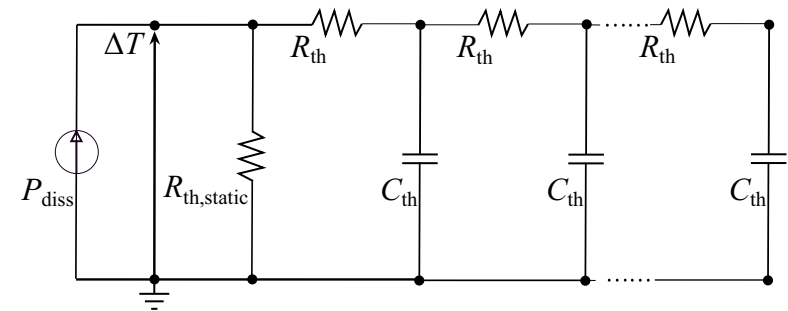
but for the simplification b is typically assumed to be zero in the literature.

Different thermal networks versus the measurements

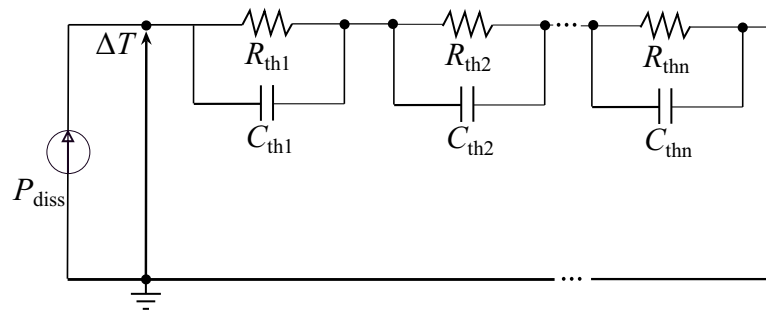
Thermal networks



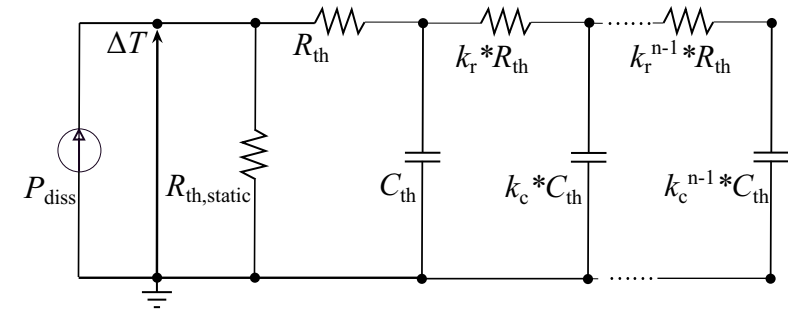
single-pole network



Nodal



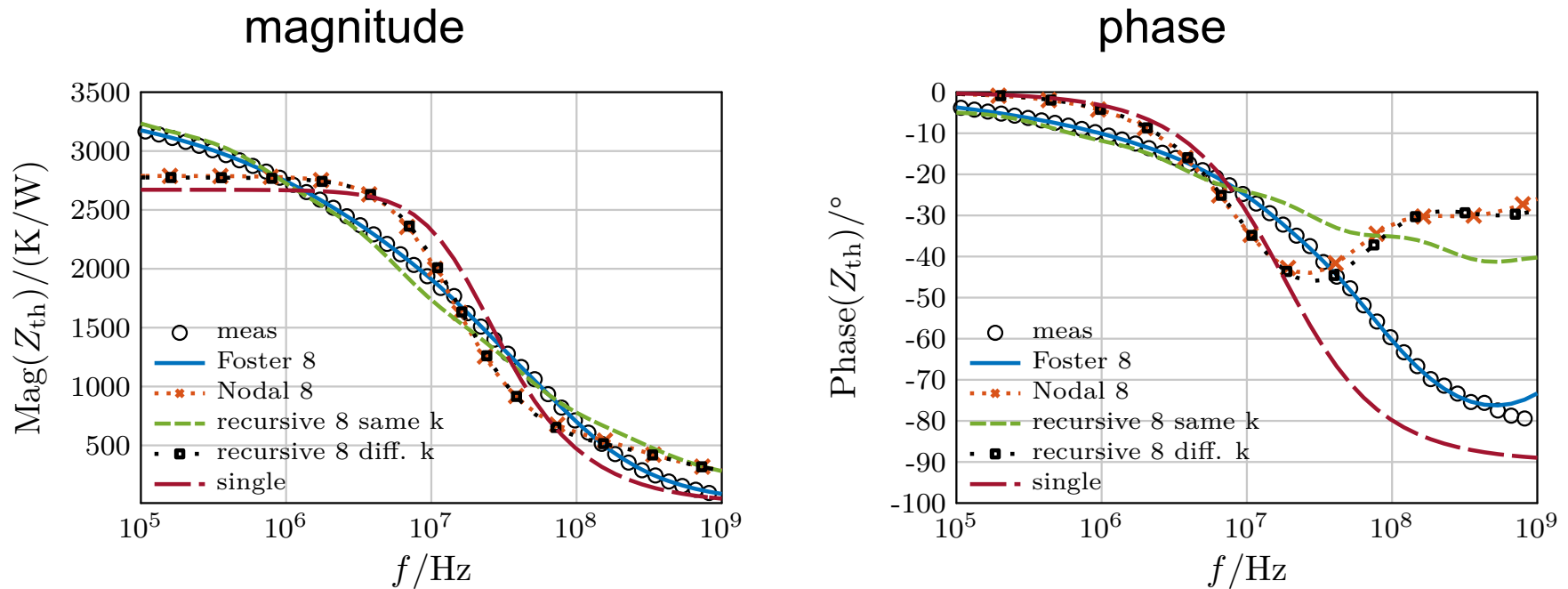
Foster



recursive

- single pole: 2 parameters;
- Foster: $2 \cdot n$ parameters;
- Nodal: 3 parameters \rightarrow simplified form of recursive model;
- recursive: 4 parameters for $k_r = k_c$, 5 parameters for $k_r < 1$, $k_c > 1$.

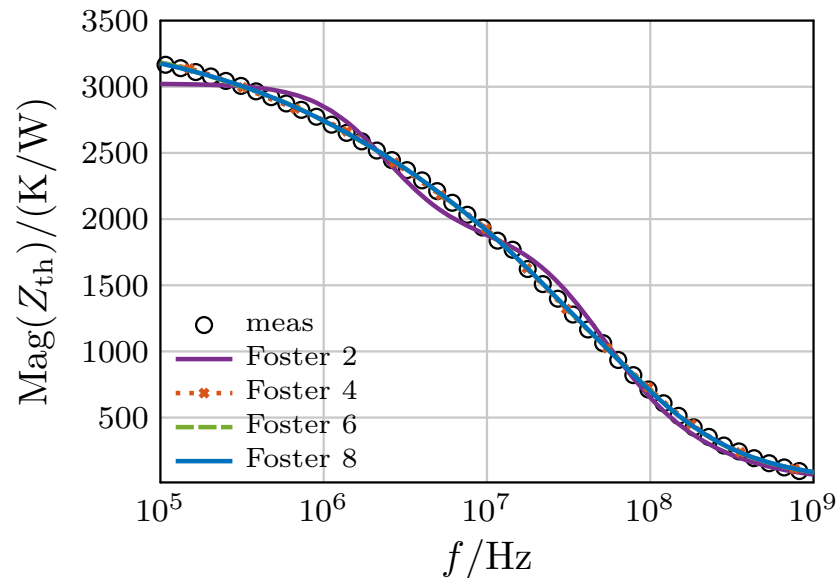
Model vs. measurement



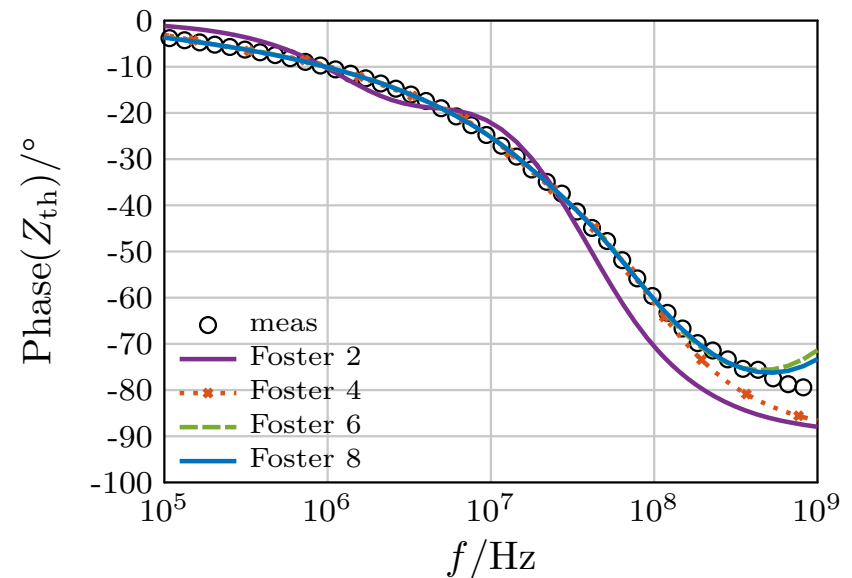
- $V_{BE}=0.94 \text{ V}$, $V_{CE}=0.75 \text{ V}$, $T=323 \text{ K}$;
- Magnitude: Foster and recursive model (same k) show a good agreement;
- Phase: Foster has the best agreement, single pole agrees reasonable, others **cannot reach phase angle below -45°**
 - EC form of nodal and recursive model do not allow a smaller degree than -45° ;
- In previous publications, **recursive model was preferable** as it had the **most accuracy** with only 4 or 5 parameters, **much less than foster model**;
- **Foster agrees best with measurements.**

Foster model with different poles

magnitude

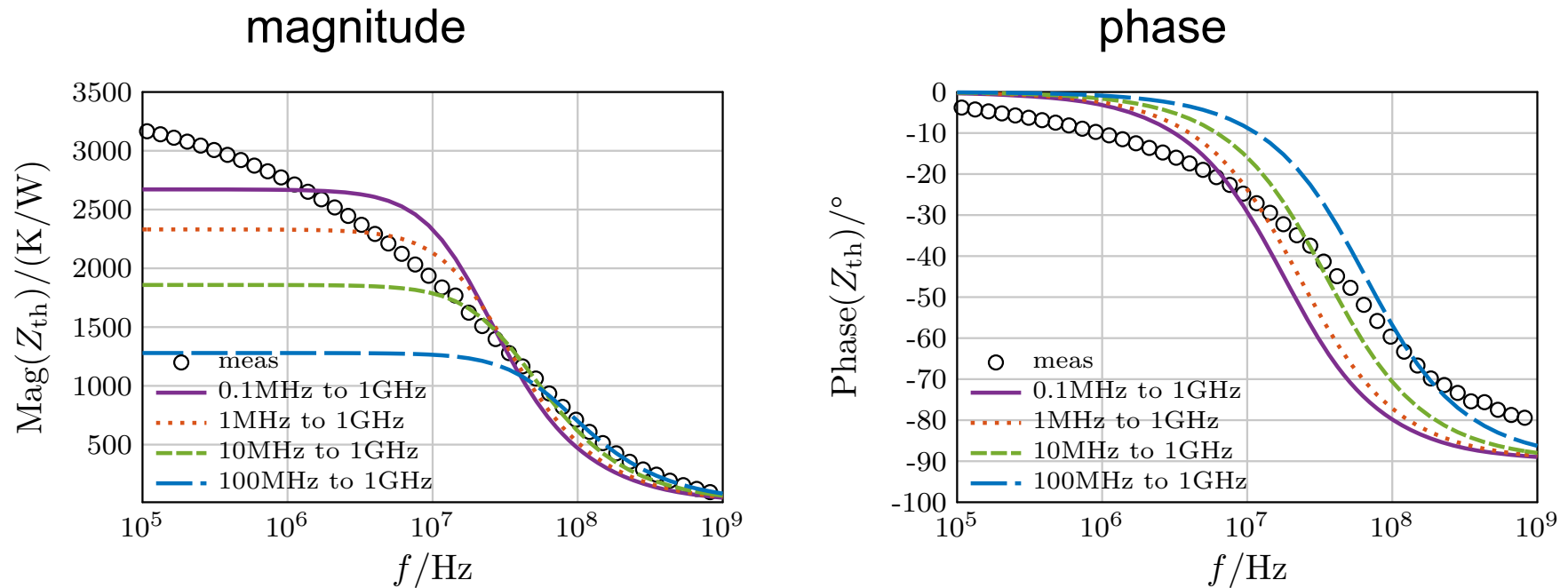


phase



- $V_{BE}=0.94 \text{ V}$, $V_{CE}=0.75 \text{ V}$, $T=323 \text{ K}$
- Foster model with different poles all show reasonable agreement with measured results;
- Model with least number of poles (2-pole Foster network) has wiggles, but is still reasonable;
- Model with 4 poles already shows very good agreement.

Single-pole model

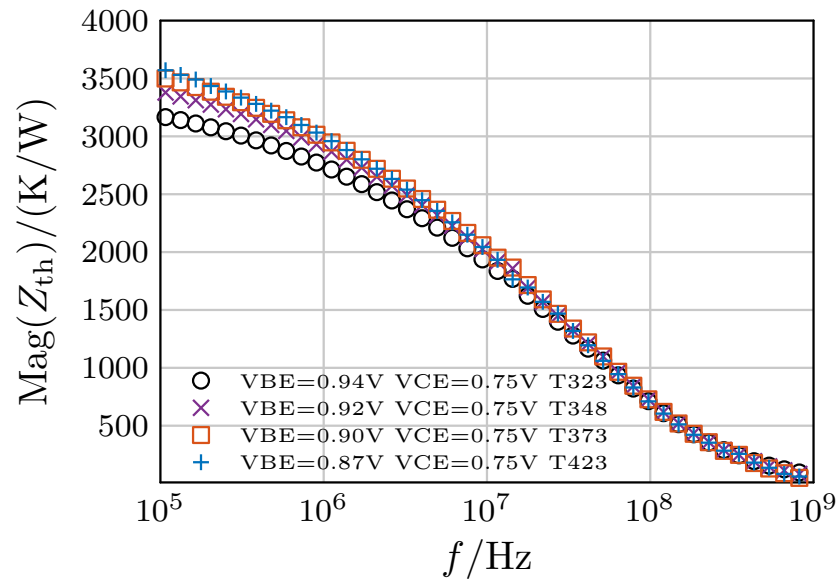


- Optimize single-pole model over different frequency ranges
 - 0.1 MHz to 1 GHz
 - 1 MHz to 1 GHz
 - 10 MHz to 1 GHz
 - 100 MHz to 1 GHz
- Magnitude can be optimized down to 10 MHz, phase can only be optimized down to 100 MHz.
- For frequency lower than 100 MHz, single-pole network is not accurate anymore.

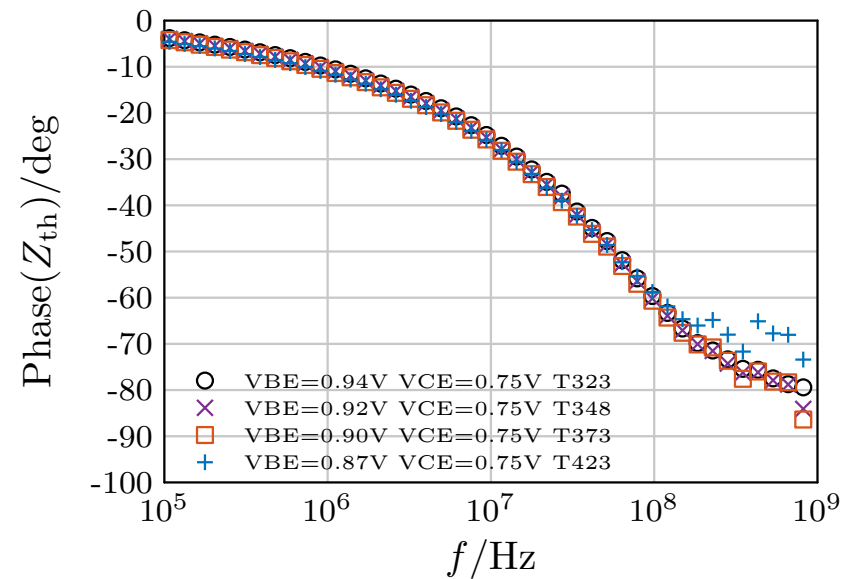
Characterization of T dependence of thermal impedance

T dependence of Z_{th}

magnitude



phase



- The I_C is around 12 mA for all T ;
- $\text{Mag}(Z_{th})$ increases with T ;
- $\text{Phase}(Z_{th})$ does not change with T .

$$R_{thi} = \int_{z_{lower}}^{z_{upper}} \frac{1}{\kappa_i A_i(z)} dz \quad \text{and} \quad C_{thi} = \int_{z_{lower}}^{z_{upper}} \frac{\kappa_i}{\alpha} A_i(z) dz$$

- ratio of imaginary and real part are T independent;
- inaccurate modeling using Nodal and recursive network;
- consistent T trend for single-pole and Foster network.

Summary

Conclusion

- The accurate thermal impedance modeling is required for **circuits at low frequency range requiring large power**;
- Uniform frequency dependence of thermal impedance and Y parameters may indicate the **uniform distribution of thermal conductivity for SG13G2**;
- The **Y -parameter method** is used to extract the Z_{th} ;
- Four thermal networks are compared with the measurement, and the favorably used **recursive network** in the previous work cannot model the thermal impedance for SG13G2 due to **its minimal phase of -45°** ;
- The **Foster network shows the best agreement**, the 2-pole Foster agrees with measured value reasonably over **0.1 MHz to 1GHz** with 4 parameters;
- **Single-pole** network can be used above **100 MHz** with great accuracy;
- The **magnitude of Z_{th} shows a T dependence, and phase of Z_{th} is T independent**, which confirms the Foster rather than recursive network as an preferable thermal network G2.

Outlook

- T dependence of C_{th} needs to be determined in single-pole thermal network;
- Determination of T dependence of the elements in multiple-pole thermal network;
- The comparison of Y-parameters between model simulation using va code and measurements needs to be done;
- CPU time between single-pole and multi-pole network need to be compared;
- Measurement, characterization and modeling of thermal impedance at cryogenic T .

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Thanks for your attention!

Any further question and discuss are welcome:

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