
HICUM/L2 version 2.34

Release Notes

August 2015

michael.schroter@ieee.org

andreas.pawlak@tu-dresden.de

Depletion capacitance grading factors

Range of the grading factors changed to exclude 1.0

- applies to all grading factors: z_{Ei} , z_{Ep} , z_{Ci} , z_{Cx} , z_S and z_{Sp} (newly introduced)

parameter real z_{ei} = 0.5 from (0:1]

changed to

parameter real z_{ei} = 0.5 from (0:1)

Conditions for noise correlation evaluation

Change requires *both alit and alqf* to be greater than 0

- Conditional statement

```
if ( flcono==1 && (alit > 0 || alqf > 0)) begin
```

changed to

```
if ( flcono==1 && (alit > 0 && alqf > 0)) begin
```

- Notes:
 - Device physics always requires both parameters to be non-zero
 - For test purposes, one or both parameters can still be set to a small value if required

Default value for forward-bias base charge Q_{bf}

Added Q_{bf} in both branches of the conditional statement

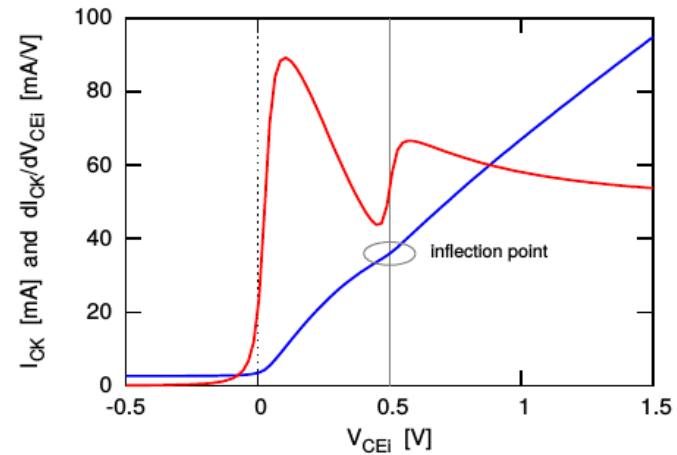
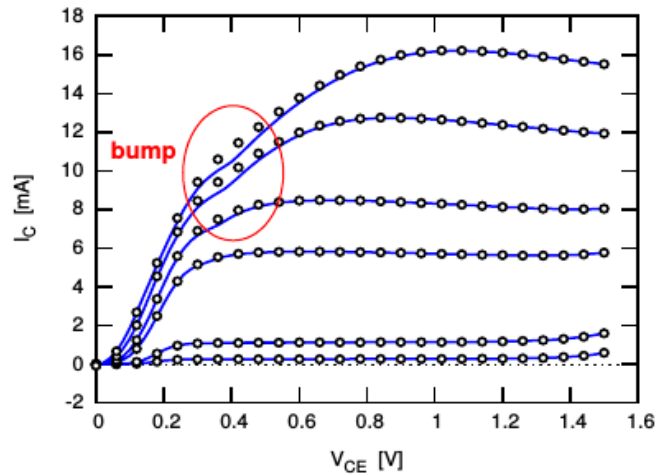
- transit time macro:

```
if(itf < 1.0e-6*I_CHK) begin\  
    Q_fT          = Q_f;\br/>    T_fT          = T_f;\br/>    Q_bf          = 0;\    <- New line included  
end else begin ...
```

=> defined value for Q_{bf} in all cases

Improved ICK formulation

- Feature request by ST [1]
 - transition of ICK from (very) low to higher voltages may cause bump



- adding a formerly fixed smoothing parameter now as model parameter a_{ick}

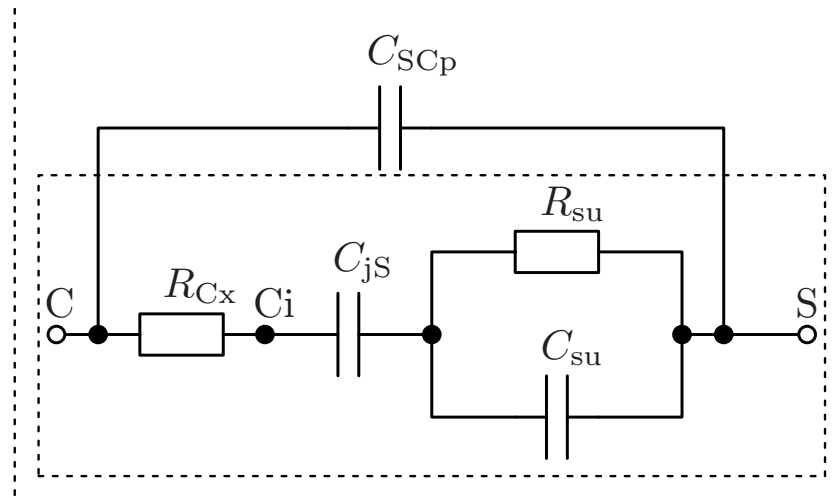
$$I_{CK} = \frac{v_{ceff}}{r_{Ci0}} \frac{1}{\left(1 + \left(\frac{v_{ceff}}{V_{lim}}\right)^{\delta_{ck}}\right)^{1/\delta_{ck}}} \left[1 + \frac{x + \sqrt{x^2 + a_{ick}}}{2} \right]$$

[1] Didier Céli, "Investigation on Bias Dependence of Critical Current ICK in HICUM Models", 27th BAK, Crolles, France, October 24, 2014

Substrate capacitance and coupling network

Extended too simple network towards more accurate representation

- Added separate Collector-Substrate perimeter related substrate capacitance C_{SCp}



- separate set of parameters: C_{SCp0} , V_{DSp} , z_{Sp} , V_{PTSp} (to allow DTI and junction isolation)
- $C_{SCp} = \text{const.}$ for $V_{DSp} = 0$ \Rightarrow trench isolation
- $C_{SCp} = f(V_{SC})$ for $V_{DSp} > 0$ \Rightarrow junction isolation
- temperature dependence via existing V_{gS} (for $V_{DSp} > 0$) or constant with T (for $V_{DSp} = 0$)

(V_{DSp} acting as flag)

Depletion capacitances

- at small z and high forward bias, $v/V_D > 1$ may occur in $(1-v/V_D)^2 \Rightarrow$ overflow
- correction term in calculation of $v_{j,m}$ to avoid $v_{j,m} > V_D$

$$v_{j,m} = -V_{jPCi} + V_r \left[\ln(1 + e_{j,m}) - \exp\left(-\frac{V_{jPCi} + V_{fCi}}{V_r}\right) \right]$$

- in the code:

$$Dv_j2 = -Dv_p + Da * \ln(1.0 + De) ; \backslash$$

changed to

$$Dv_j2 = -Dv_p + Da * (\ln(1.0 + De) - \exp(-(Dv_p + DV_f) / Da)) ; \backslash$$

- caused by residual value of smoothing function $\ln[1+\exp(v)]$ for $v \rightarrow \infty$
 - for calculating the offset, a series expansion of $\ln(y)$ with $y=1+x$ at x is applied

$$\ln(1+x) = \ln(x) + \frac{1}{x} - \frac{1}{2x^2} + \frac{1}{3x^3} - \dots = \ln(x) + \sum_{k=1}^{\infty} (-1)^{k+1} \frac{1}{kx^k}$$

- note, when stopping the series after an odd k , an overestimation is obtained thus, using only the linear term provides a safe estimate of the offset

Output resistance calculation (OP only)

bug fix in adding avalanche related term

- Wrong sign for the conductance corresponding to avalanche breakdown
- Code for gAVL

```
gAVL = -type*ddx(iavl, V(ci));  
ROi  = 1/(gOi+gAVL+`Gmin);
```

changed to

```
gAVL = type*ddx(iavl, V(ci));  
ROi  = 1/(gOi+gAVL+`Gmin);
```