

# 1 Model evaluation for Technology E

## 1.1 Device information

The provided device is a 12GHz transistor fabricated in a BiCMOS foundry process. The transistor size is  $0.6 \times 4.8 \mu\text{m}^2$ .

- The provided data consists of
  - de-embedded S-parameters as a function of bias and frequency for  $V_{BC} = \text{const}$  (various values);  $T = 21.4\text{C}$  is given as information in respective file headers.
  - DC bias data, measured on the same device and for same  $V_{BC}$ , but at a different temperature  $T=24.2$ .

## 1.2 Parameter extraction

The de-embedded S-parameter data (incl. bias information) were converted to y-parameters. In particular, data with constant  $f = 1\text{GHz}$  were derived for the determination of  $f_T$  and an overall comparison of y-parameters over bias. For parameter extraction, only the consistent data set from S-parameter measurements (“AC” data) were employed to avoid having to deal with different temperatures during extraction and fine-tuning (changing temperature would increase effort, time and error probability during extraction). However, the same parameters were then also used, with some of them adjusted according to the additional information available at lower current densities, to compare the DC data (obtained from pure DC measurements) at the corresponding temperature.

Junction capacitance data (containing depletion and isolation components) were obtained from “cold” measurements. Figs. 1.2/1 to 1.2/3 show the comparison between measured data (symbols) and model (lines). Note the extended scale by suppressing the y-axis origin.

Substrate transistor action seemed to be negligible, and the corresponding parameters were omitted.

Below, first the results obtained for the AC data set are shown, followed by the results for the DC data set (and additional comments). In many cases the data are plotted vs. the (log of) collector current density  $I_C/A_E$  rather than vs.  $V_{BE}$ . The latter is of little interest and use for circuit design, and does not provide circuit design related information on the bias point. Note, that  $V_{BE} \sim \log(I_C)$  for low current densities.

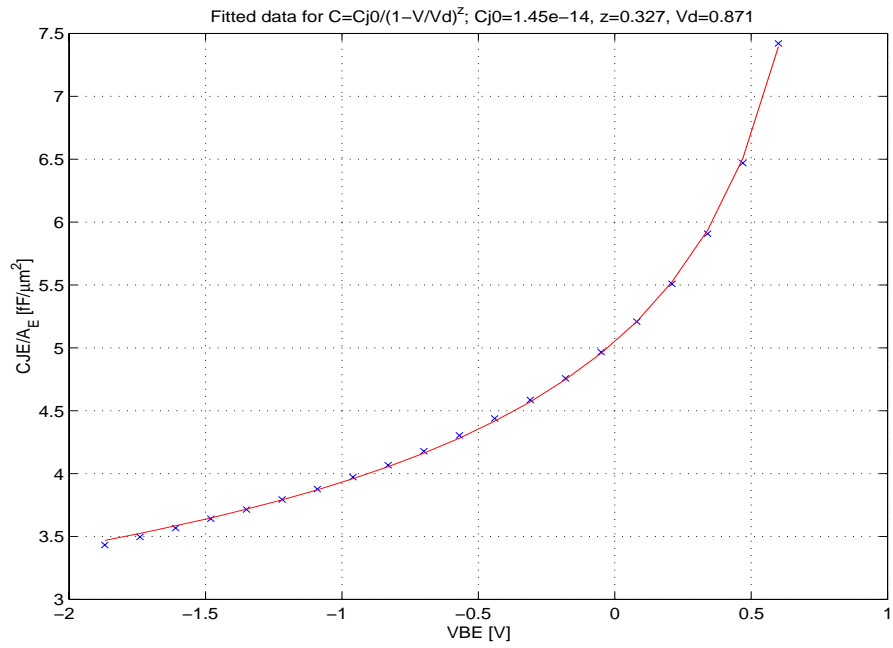
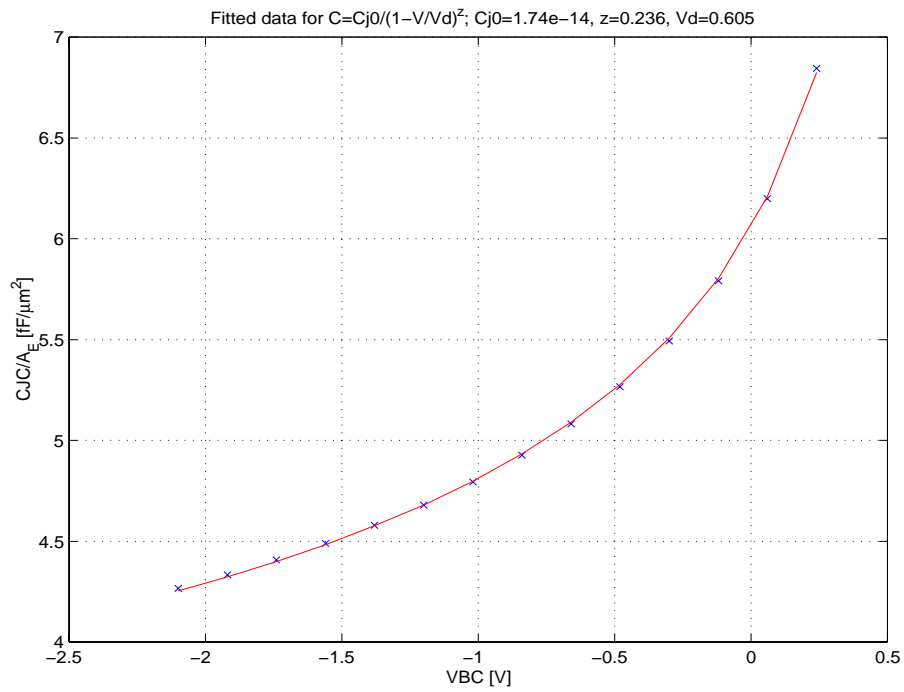


Fig. 1.2/1: Base-emitter capacitance vs.  $V_{BE}$ : measurement (symbols), HICUM (line).



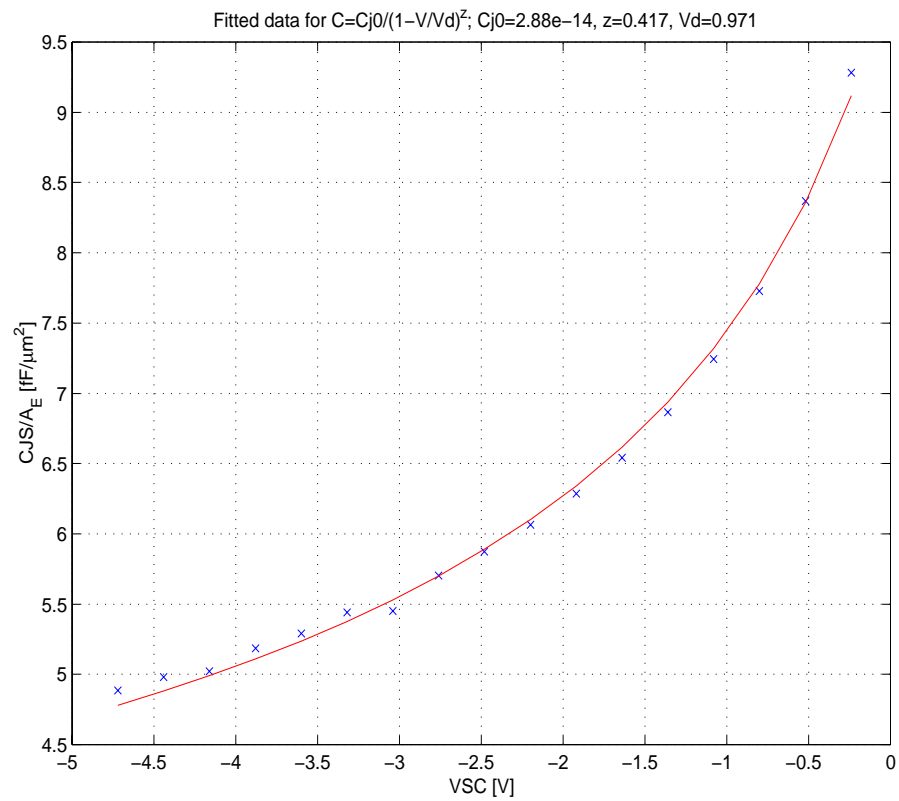


Fig. 1.2/3: Collector-substrate capacitance vs.  $V_{SC}$ : measurement (symbols), HICUM (line).

### 1.3 Results for the AC measurement data (T=21.4C)

Figures 1.3/1 to 1.3/3 contain a comparison of standard characteristics between model (solid lines) and measurements (symbols) within the interesting and available collector current density range. In all cases, fairly good agreement has been obtained at least up to the current density where  $f_T$  peaks. At very high current densities, slight deviations can be observed for the base current. Such deviations can be caused by uncertainties in, e.g., series resistances, self-heating and associated temperature coefficients.

Fig. 1.3/5 shows the y-parameters as a function of collector current density at  $f = 1\text{GHz}$  and constant  $V_{BC}$  values. Excellent agreement is obtained for almost all curves.

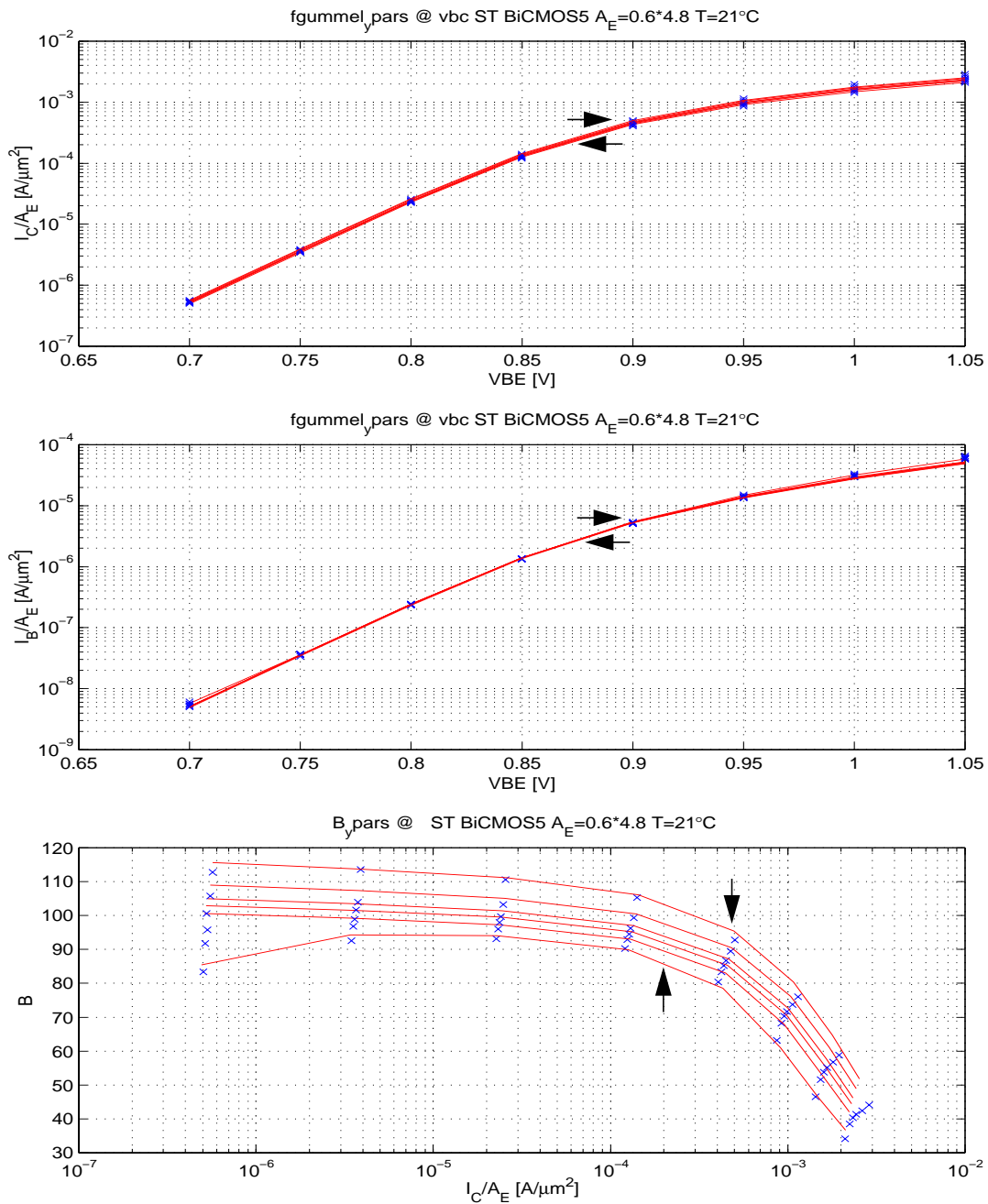
Figures 1.3/6 to 1.3/9 contain comparisons of frequency dependent y-parameters for selected bias points. In the first two figures, a set of curves was picked for  $V_{BC} = 0.5\text{V}$ , which is an extreme case, especially at high current densities: Fig. 1.3/7 shows fairly good results for a current density, that is close to  $f_T$  peak. In the last two figures, the curves were selected for the highest available (reverse) voltage  $V_{BC} = -3\text{V}$  in order to demonstrate the capability of HICUM to cover a larger bias range without loss of accuracy. For both voltages, the agreement at the lower current densities (Figs. 1.3/6 and 1.3/8) is also quite good.

At low frequencies, the measurement uncertainty does not always allow a clear conclusion. For the transistor provided, a simple substrate resistance HICUM seems to be sufficient for accurate modeling of the substrate coupling in  $y_{22}$ .

In summary, all characteristics show acceptable agreement even beyond peak  $f_T$ .

The combination of model parameter values found during fitting (cf. Fig. 1.3/10) describes the characteristics in the operating regions of interest quite well, but can be improved in some regions if additional measured data and proper test structures would be available to separate various physical as well as geometry related effects.

Note that (a)  $f_T$  peaks - depending on  $V_{BC}$  - between  $J_C$  values of 0.2 and 0.5  $\text{mA}/\mu\text{m}^2$ ; (b) operation beyond peak  $f_T$  is of interest only for circuits switching at high-speed, in which the dynamic base current can become much larger than the DC base current, making accurate DC base current modeling irrelevant compared to accurate modeling of charges which is reflected by  $f_T$  and in some cases also by, e.g.,  $f_{\text{max}}$ .



**Fig. 1.3/1:** Collector current density vs.  $V_{BE}$ , Base current density vs.  $V_{BE}$ , Current gain vs. collector current density for  $V_{BC}/V = 0.5, 0, -0.5, -1, -2, -3$ ;  $T=21.4\text{C}$ . Data source: AC measurements. The arrows indicate peak  $f_T$  for the lowest and highest  $V_{BC}$  value

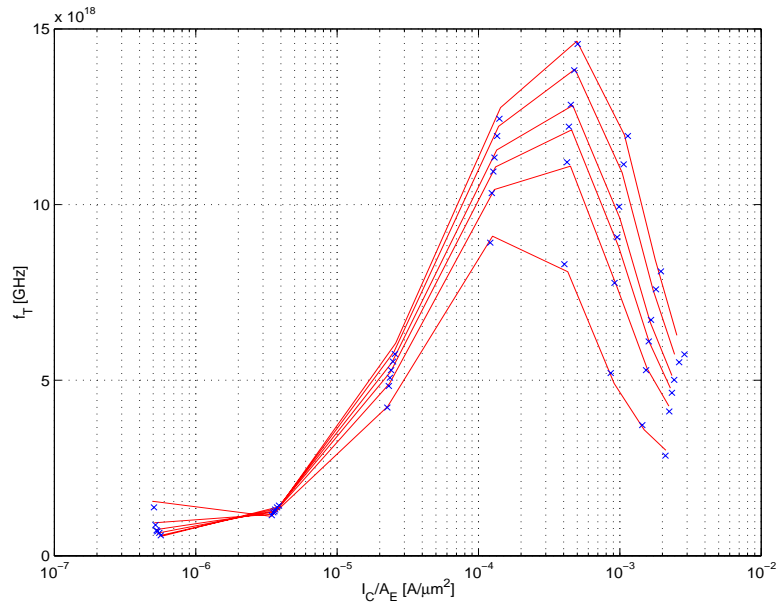


Fig. 1.3/2: Extracted transit frequency vs. collector current density for  $V_{BC}/V = 0.5, 0, -0.5, -1, -2, -3$ ;  $T=21.4$ ; model bias points according to the provided measurements

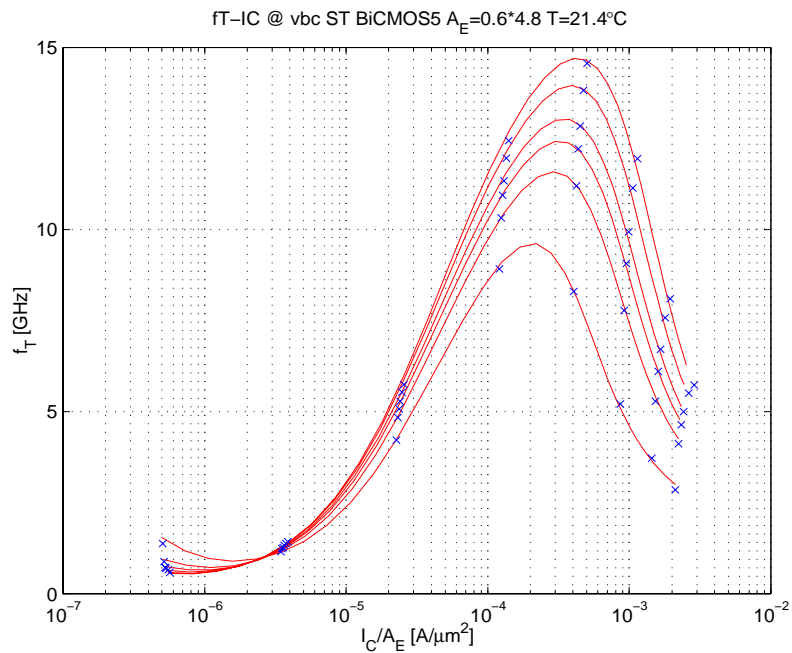


Fig. 1.3/3: Simulation for  $f_T$  with more model bias points for smoothing

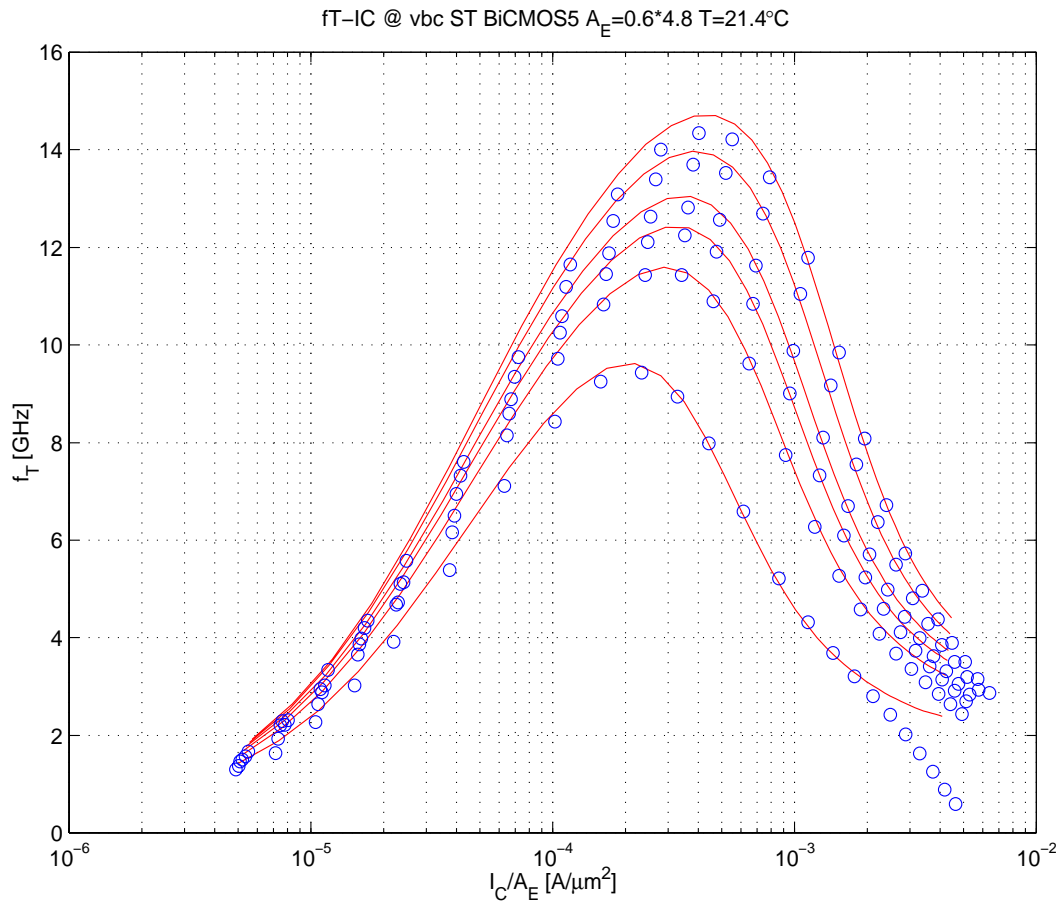


Fig. 1.3/4: Transit frequency vs. collector current density for  $V_{BC}/V = 0.5, 0, -0.5, -1, -2, -3$ ;  $T=21.4$ ; measured  $f_T$  determined from y-parameters; simulation with AC model parameters.

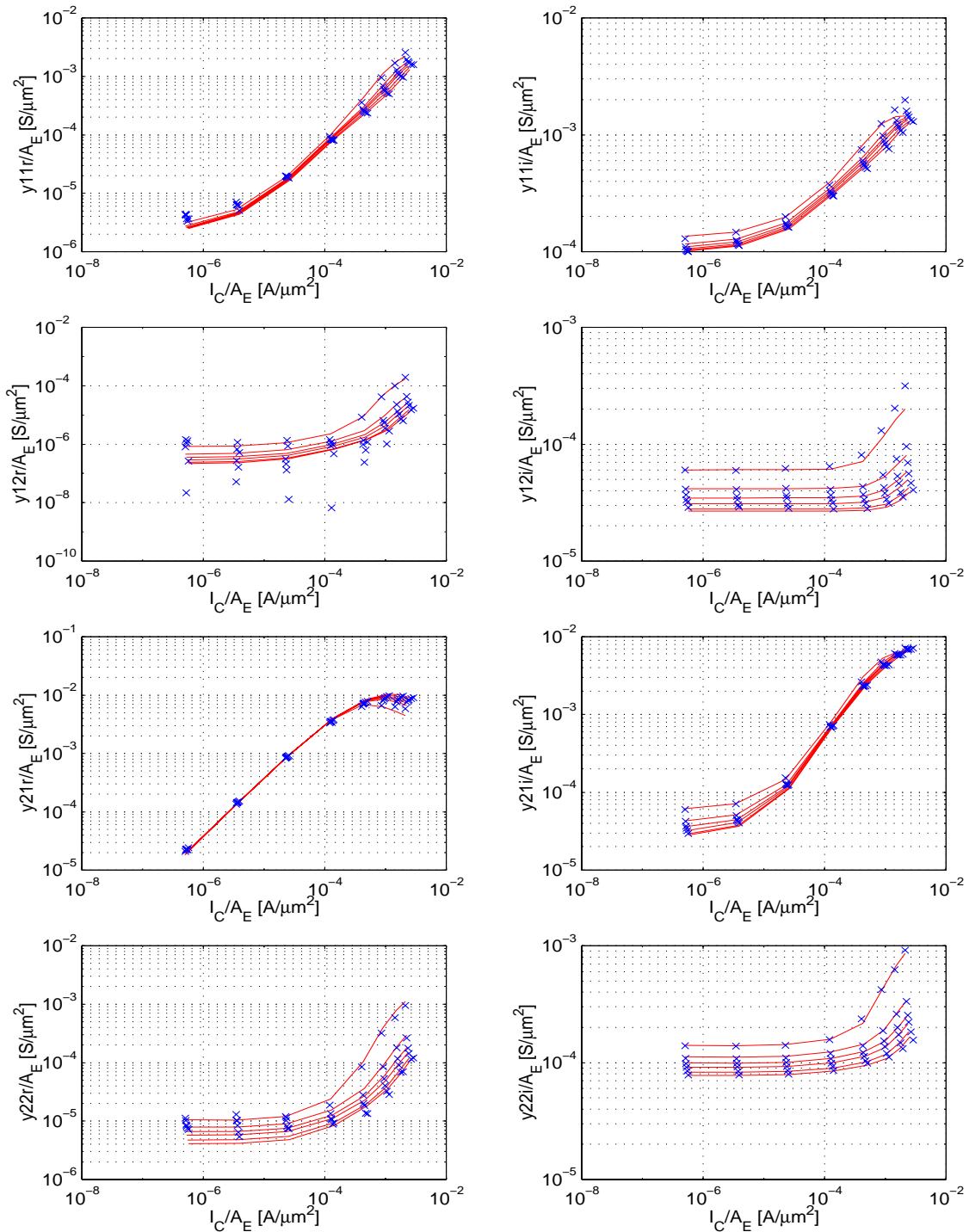


Fig. 1.3/5: Y-parameters vs. collector current density at  $f=1\text{GHz}$ ;  $V_{BC}/V = 0.5, 0, -1, -3$ ;  $T=21.4\text{C}$ .



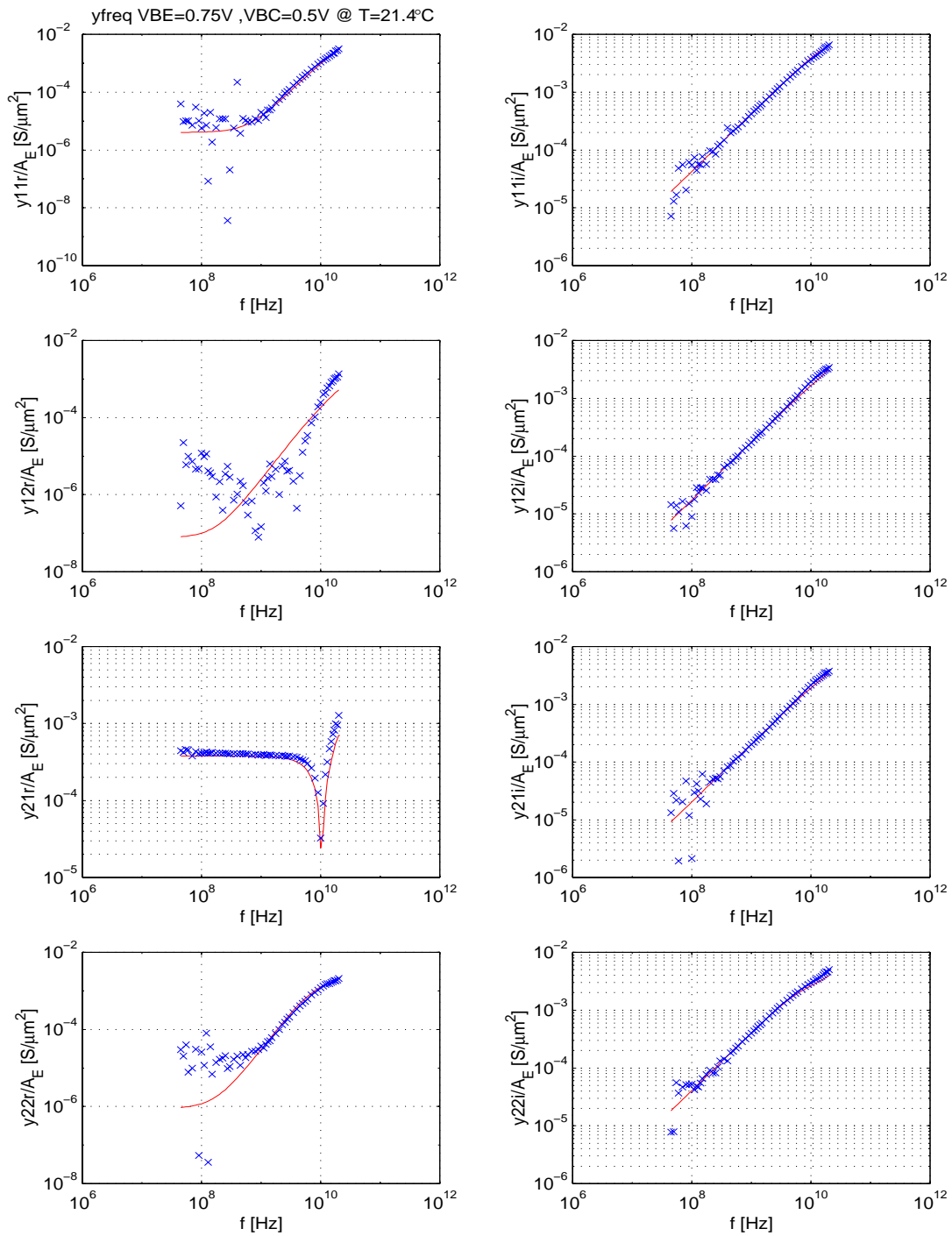


Fig. 1.3/6: Frequency dependent y-parameters at  $V_{BC} = 0.5V$  and  $I_C/A_E$  below peak  $f_T$ .

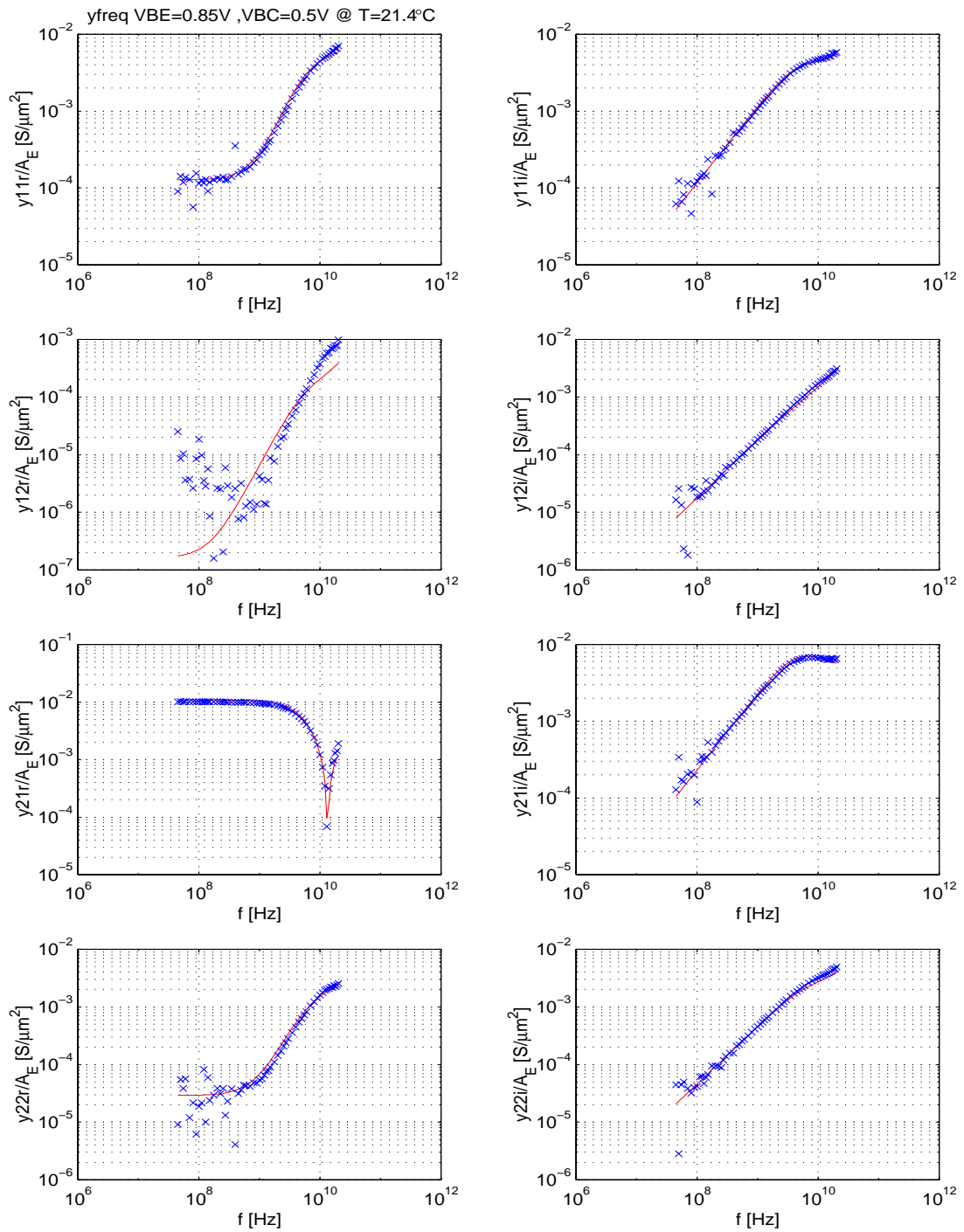


Fig. 1.3/7: Frequency dependent y-parameters at  $V_{BC} = 0.5V$  and  $I_C/A_E$  close to peak  $f_T$ .

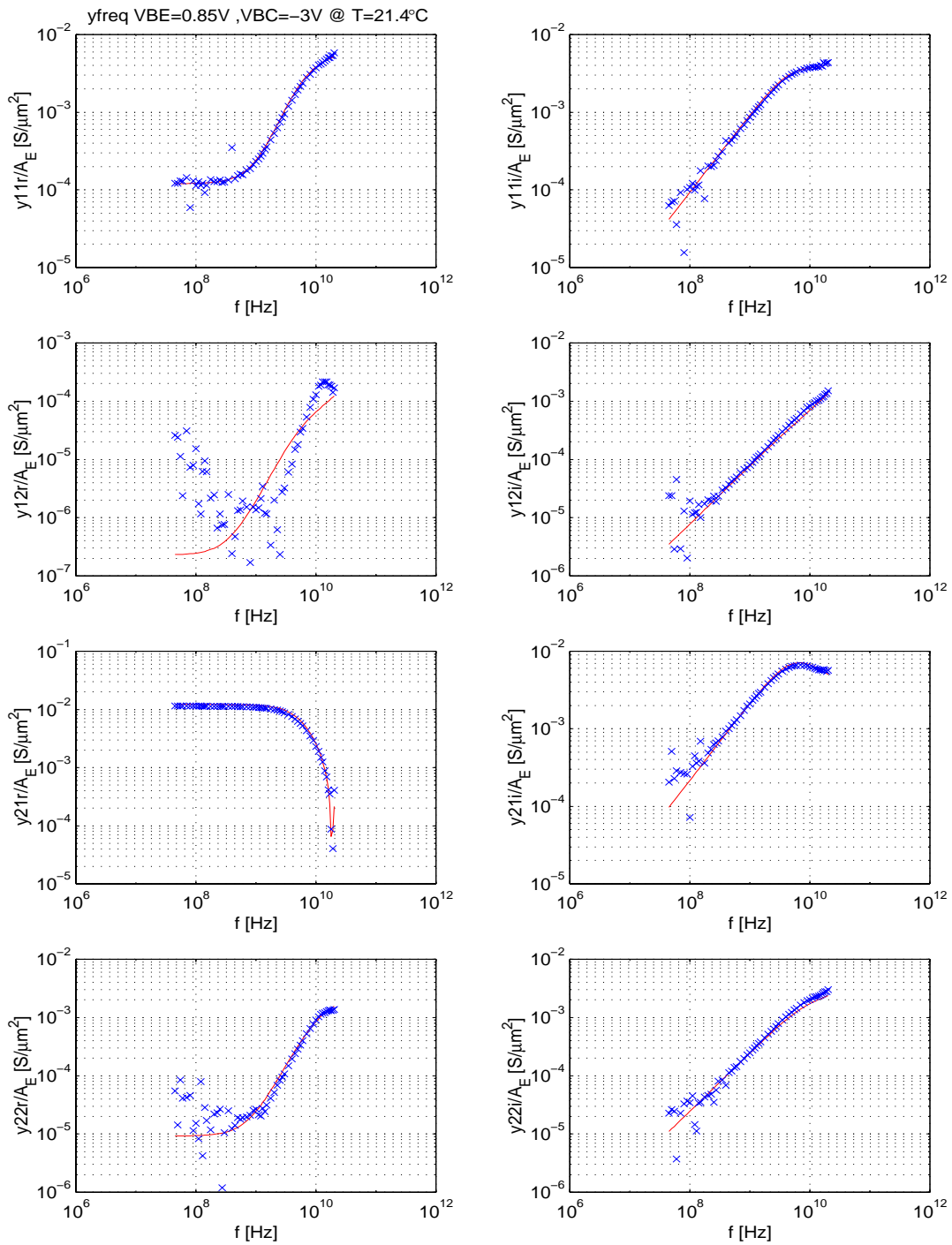


Fig. 1.3/8: Frequency dependent y-parameters at  $V_{BC} = -3V$  and  $I_C/A_E$  below peak  $f_T$ .

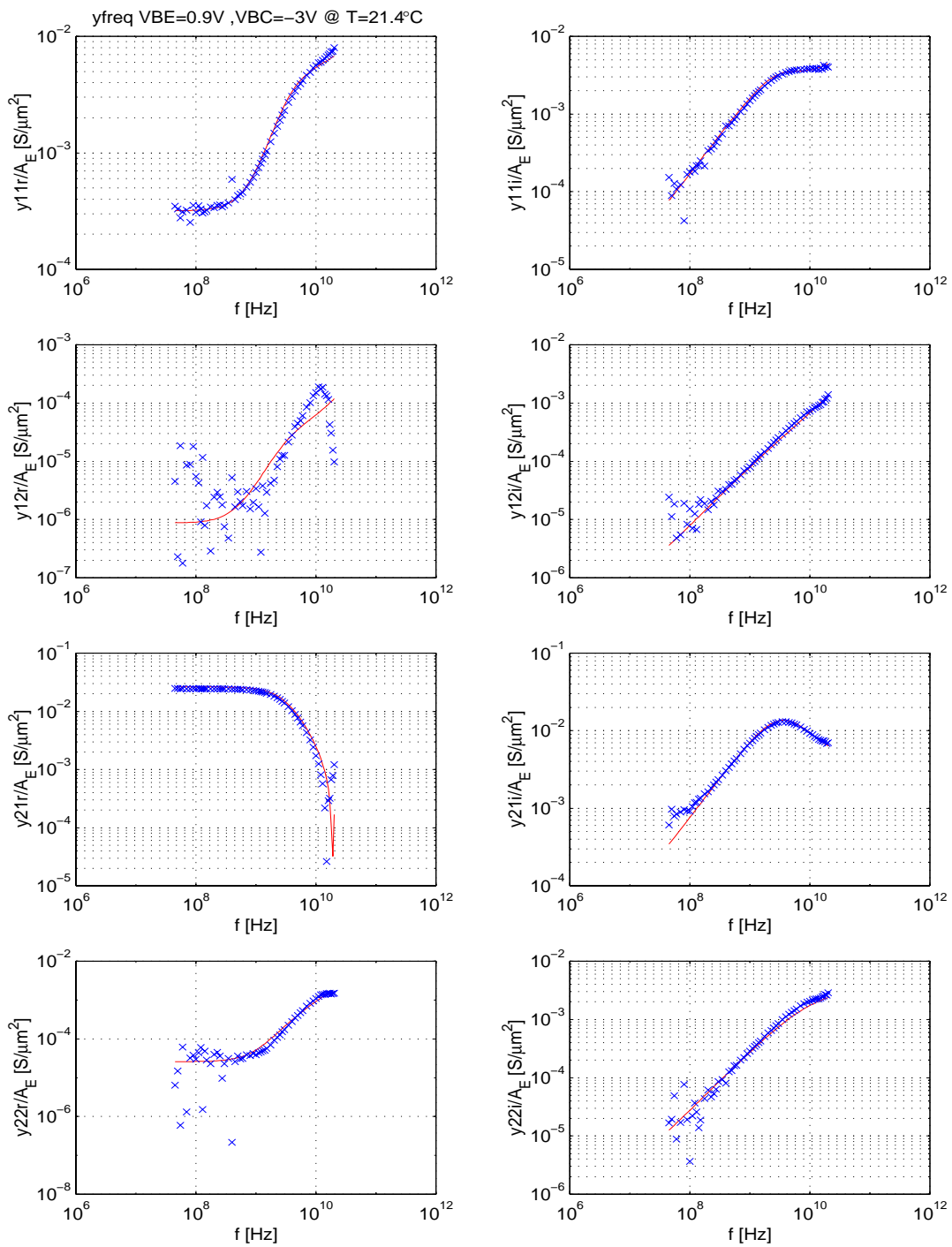


Fig. 1.3/9: Frequency dependent y-parameters at  $V_{BC} = -3\text{V}$  and  $I_C/A_E$  at peak  $f_T$ .

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** HICUM / LEVEL2 AC-Satz
'MODQ' 'Tref' 1
&HICUM2 c10=4.78E-32 qp0=2.25E-14 ich=5.20E-03 hfc= 0.20
hfe= 1.00 hjci= 0.77 hjei= 1.00 alit=0.450
cjei0=8.88E-15 vdei=0.960 zei=0.595 aljei= 2.20
cjc0=2.12E-15 vdc0=0.780 zci=0.474 vptci=1.05E+01
t0=1.02E-11 dt0h=-1.170E-12 tbvl=5.300E-13 tef0=2.55E-13
gtfe= 1.00 thcs=5.9E-11 alhc= 8.143 fthc= 0.800
alqf=0.225
rci0=4.5E+01 vlim= 0.387 vpt= 4.19 vces= 0.100
tr=0.00E+00
ibeis=1.89E-20 mbei=1.0080 ireis=7E-17 mrei=2.0000
ibcis=1.00E-30 mbci=1.0240
favl=3.000 qavl=4E-14
rbi0= 125.50 fdqr0=0.200 fgeo=0.7570 fqi=1.0000
fcrbi=0.20
latb=3.470E+00 latl=0.434
cjep0=7.95E-15 vdep=0.980 zep=0.437 aljep= 2.30
ibeps=1.00E-30 mbep=1.0110 ireps=1.00E-30 mrep=2.0000
ibets=0.00E+00 abet= 0.00
cjc0=1.42E-14 vdc0=0.835 zc0=0.452 vptc0=2.30E+00
ccox=2.78E-15 fbc=0.128
ibcx0=1.3E-18 mbcx=1.045
ceox=1.13E-15 rbx= 76.19 re= 15.500 rcx= 16.75
itss=1.00E-30 msf=1.000 tsf=0.00E+00
iscs=1.00E-30 msc=1.000
cjs0=4.01E-14 vds=0.650 zs=0.282 vpts=1.00E+03
rsu= 500.0 csu=0.00E+00
kf=0.00E+00 af=1.00E+00
vgb= 1.160 alb= 1.60E-03 alt0= 0.00E+00 kt0= 0.00E+00
zetaci= 1.600 alvs=1.00E-03 alces=4.00E-04 zetarbi= 0.830
zetarbx= 0.180 zetarcx= 0.190 zettare= -0.800
alfav=8.25E-05 alqav=1.96E-04
rth= 400.0 cth=0.00E+00 &end

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Fig. 1.3/10: Set of model parameters for the AC measurement based comparison (DEVICE).

## 1.4 Comparisons to measured DC data (T= 24.2C)

Figure 1.4/1 contains a comparison of DC characteristics between model (solid lines) and measurements (symbols). These DC data cover a larger bias range towards *very low* current densities but contain, in contrast to the data from AC measurements, only a subset of  $V_{BC}$  values. For the comparison, most model parameters (cf. Fig. 1.4/8) were left unchanged from the previous (“AC”) values, except the ones modeling the various base current components at low current densities and the avalanche current, for which insufficient data was available from “AC” measurements. The current gain drops at much lower current densities compared to the data from AC measurements, requiring to re-adjust the corresponding base current parameters. In general, similar agreement is obtained for the same characteristics that were already compared for the data set from AC measurements. Also, good agreement is obtained for the bias region at very low current densities.

In addition to the usual DC characteristics, several low-frequency derivatives, i.e. (normalized) conductances, are shown.

- Fig. 1.4/2a, the normalized transconductance

$$\frac{g_m}{I_C} = \frac{1}{I_C} \left. \frac{dI_C}{dV_{BE}} \right|_{V_{BC}} . \quad (1.4.0-1)$$

The observed deviations might be due to insufficient information on the partitioning of internal and peripheral base emitter capacitance which cannot be obtained from a single device.

- Fig. 1.4/2b, the normalized input conductance

$$\frac{g_{BE}}{I_B} = \frac{1}{I_B} \left. \frac{dI_B}{dV_{BE}} \right|_{V_{BC}} \quad (1.4.0-2)$$

- The deviations at very high current densities can be due to the unknown partitioning of various effects (as already discussed before) and would need further investigation. However, the importance of the above characteristic for circuit design is unclear.
- In Fig. 1.4/3b, the output conductance:

$$g_o = \left. \frac{dI_C}{dV_{CE}} \right|_{I_B} . \quad (1.4.0-3)$$

The agreement is fairly good over the entire bias range. Deviations are believed mainly to be due to (a) insufficient knowledge about the voltage dependence of the internal BC junction capacitance (cannot be extracted from a single device) and other relevant parameters, and (b) the weak avalanche model that does not take into account the breakdown mechanism at high current densities (which occurs close to the buried layer).

All derivatives were obtained by numerical differentiation.

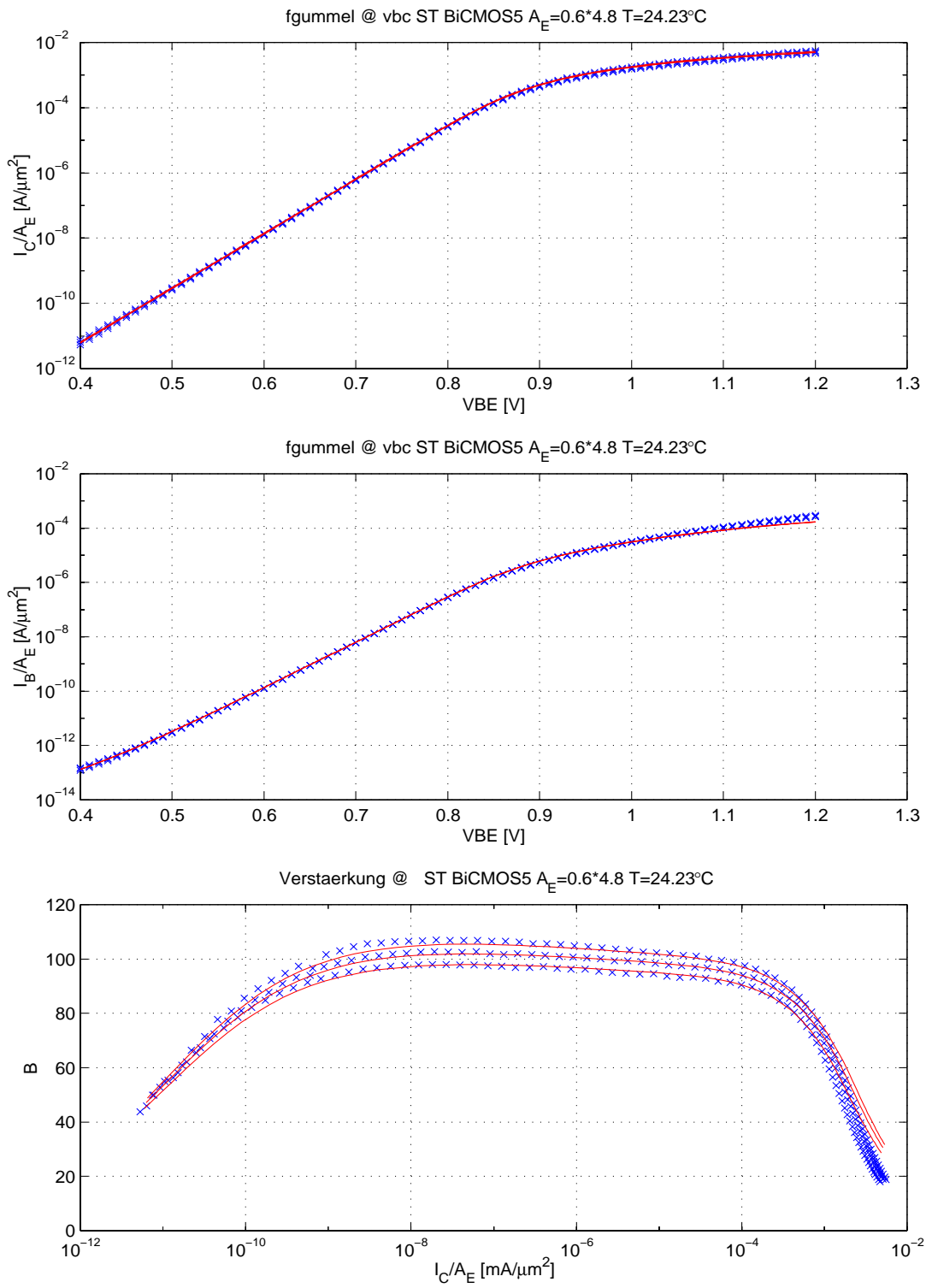


Fig. 1.4/1: Forward gummel characteristics and DC current gain for  $V_{BC}/V_{BE} = 0, -1, -2$ ;  $T=24.2^\circ\text{C}$ .  
Data source: DC measurements.

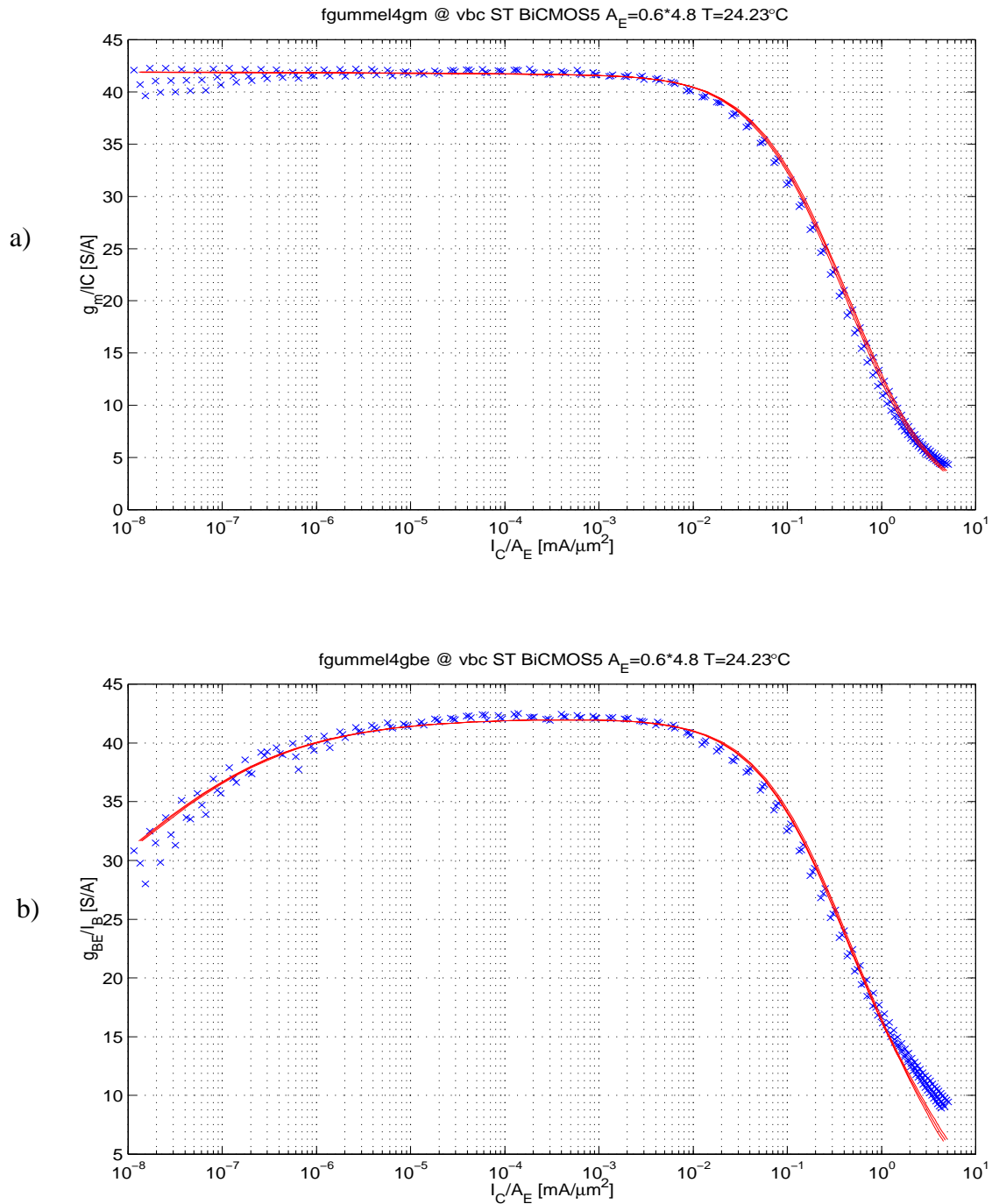
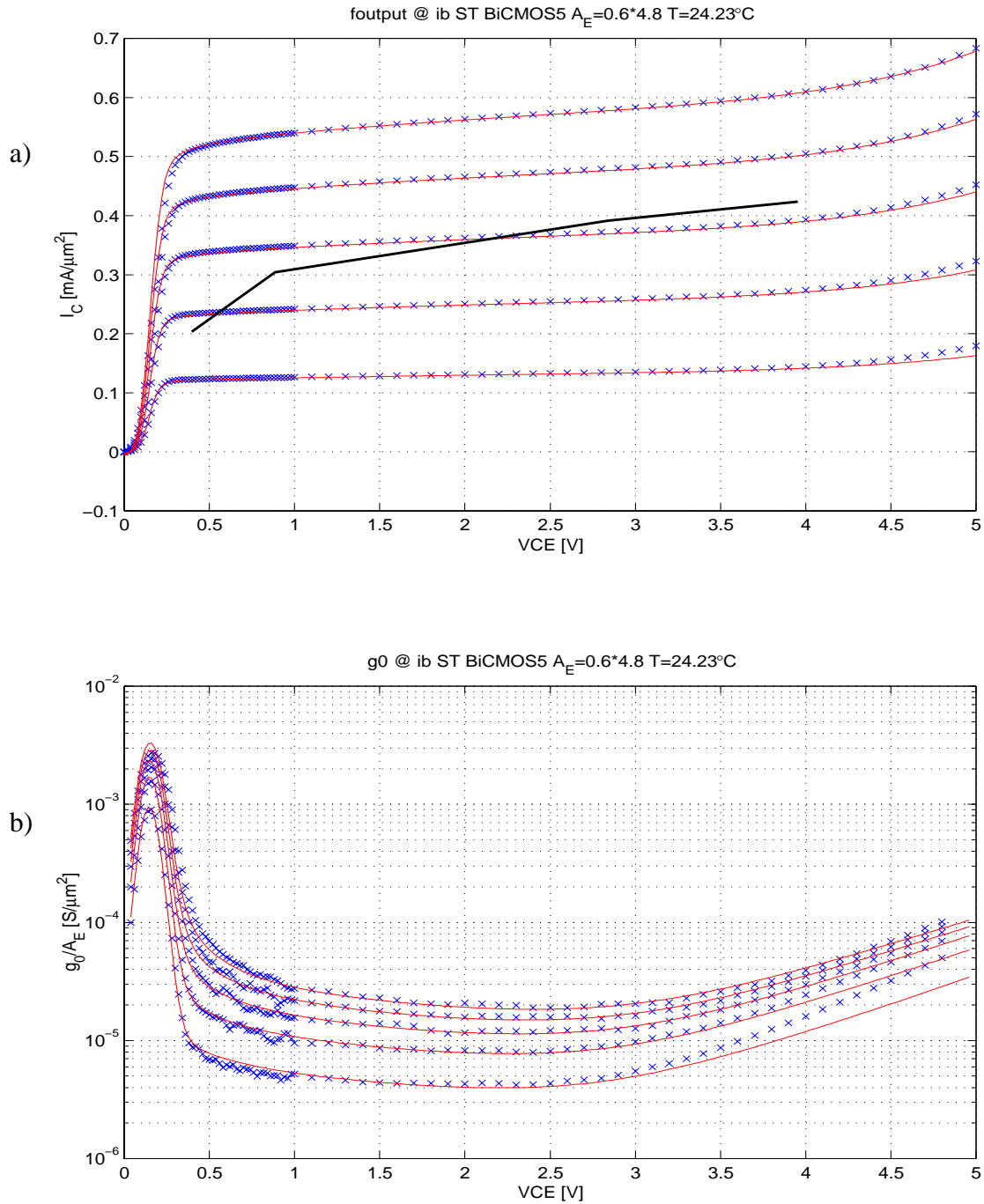


Fig. 1.4/2: Low-frequency transconductance and input conductance vs. collector current density;  $V_{BC}/V = 0, -1, -2$ ;  $T=24.2\text{C}$ . Data source: DC measurements.





**Fig. 1.4/3:** Output characteristics and output conductance for  $I_B/\mu\text{A} = 4, 8, 12, 16, 20$ ;  $T = 24.2^\circ\text{C}$ .

Data source: DC measurements.

The line indicates the current densities at which  $f_T$  peaks.

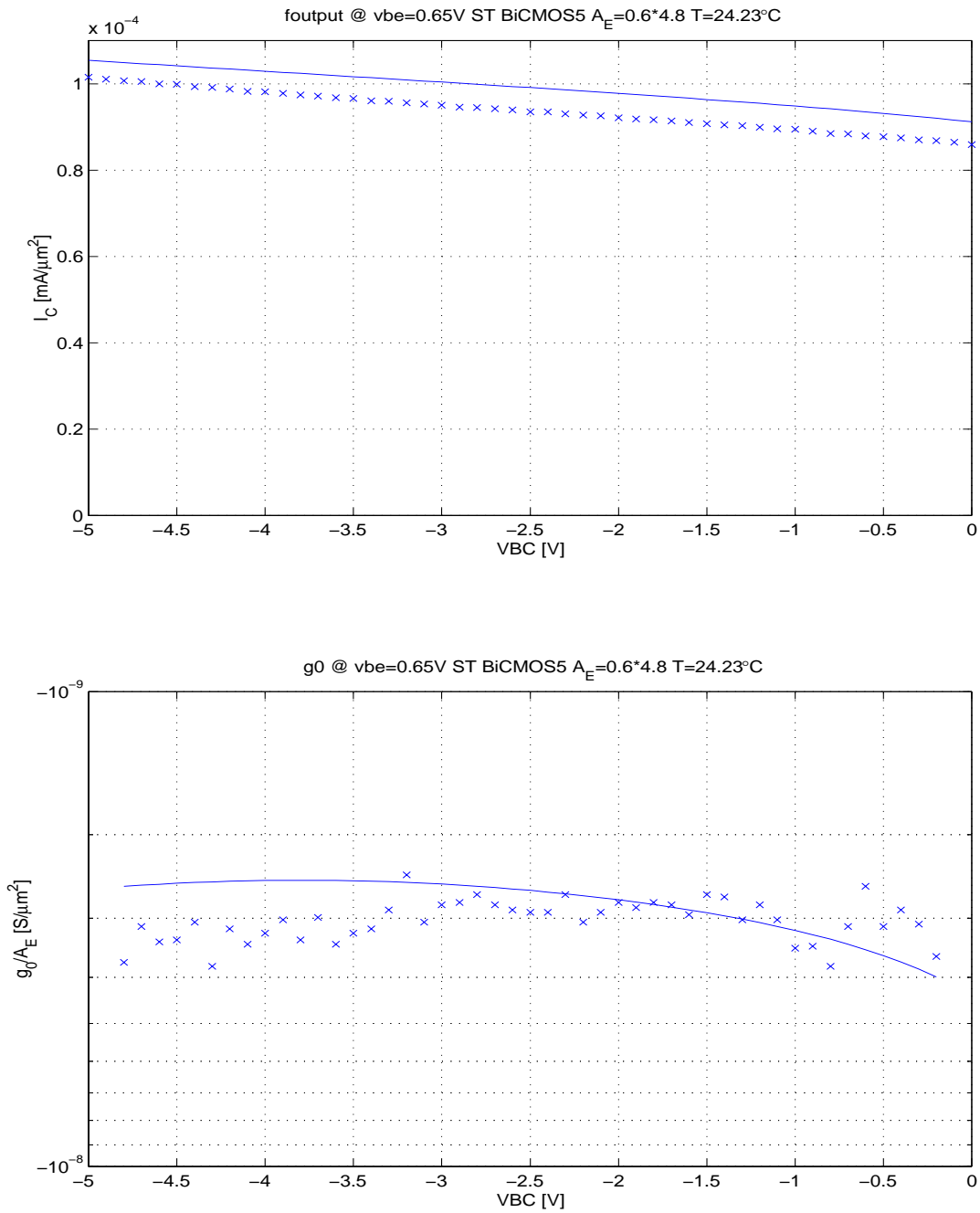


Fig. 1.4/4: Output characteristics and output conductance for  $V_{BE}/V=0.65$ ;  $T=24.2C$ .  
Data source: DC measurements.

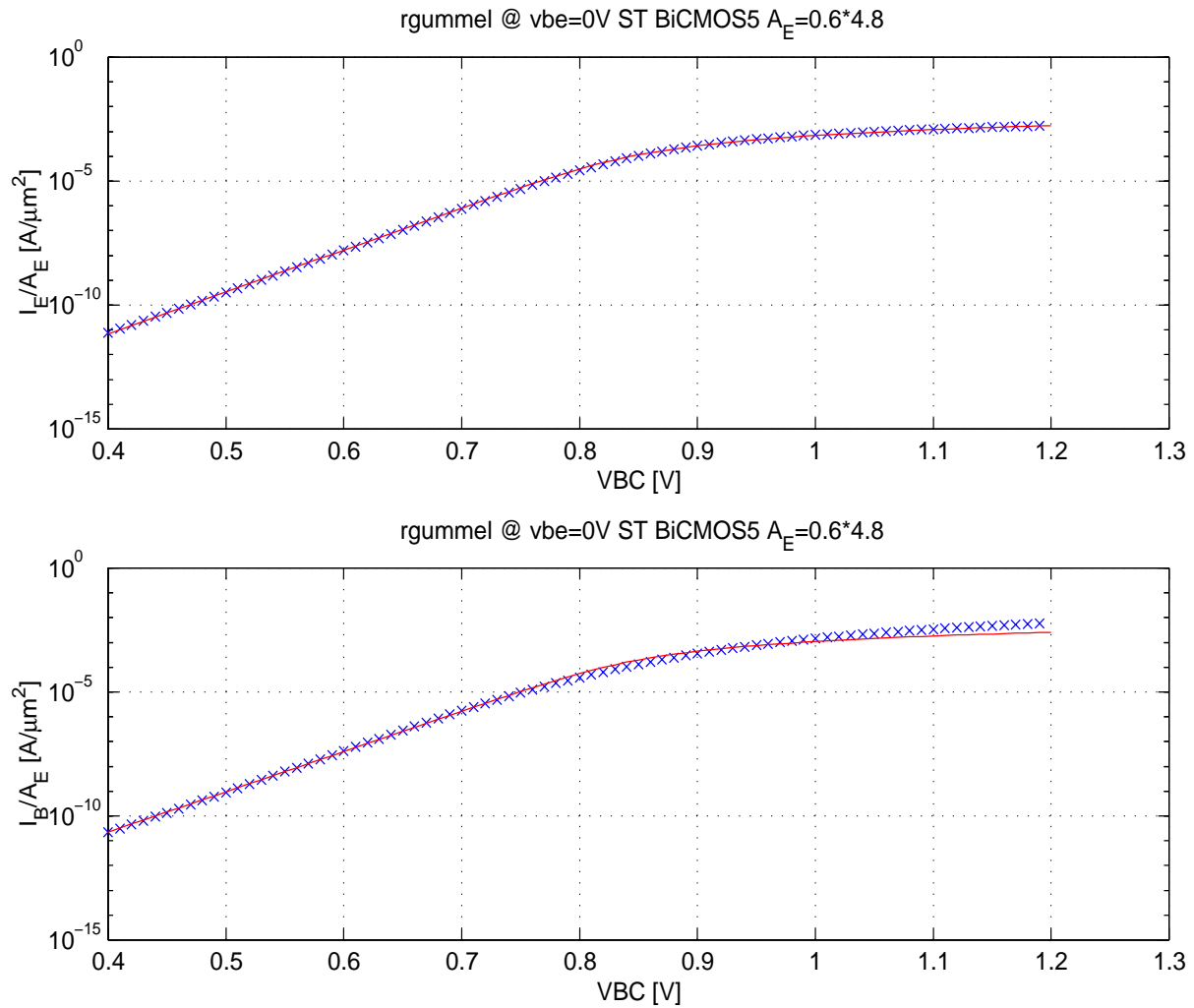


Fig. 1.4/5: Reverse gummel plots for  $V_{BE}/V=0$ ;  $T=24.2\text{C}$ .

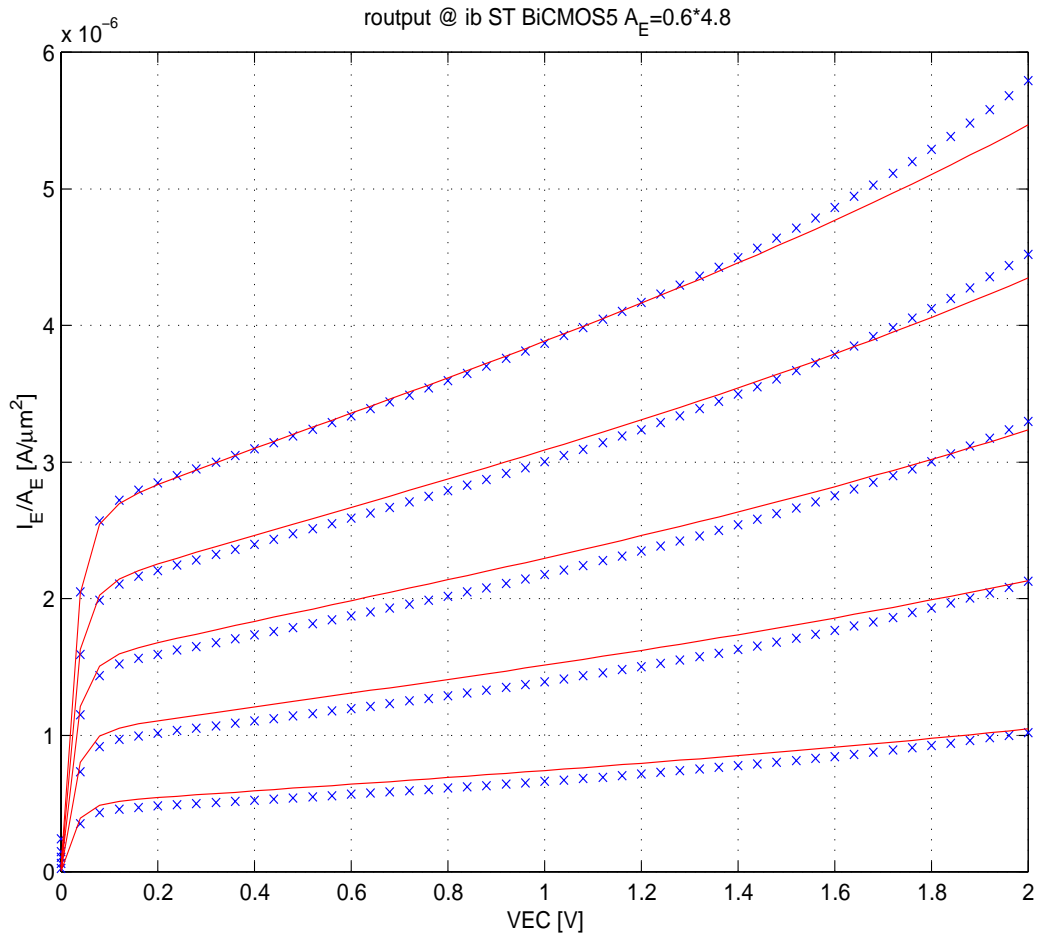


Fig. 1.4/6: Reverse output characteristics for  $I_B/\mu\text{A}=4, 8, 12, 16, 20$ ;  $T=24.2\text{C}$   
 Data source: DC measurements.

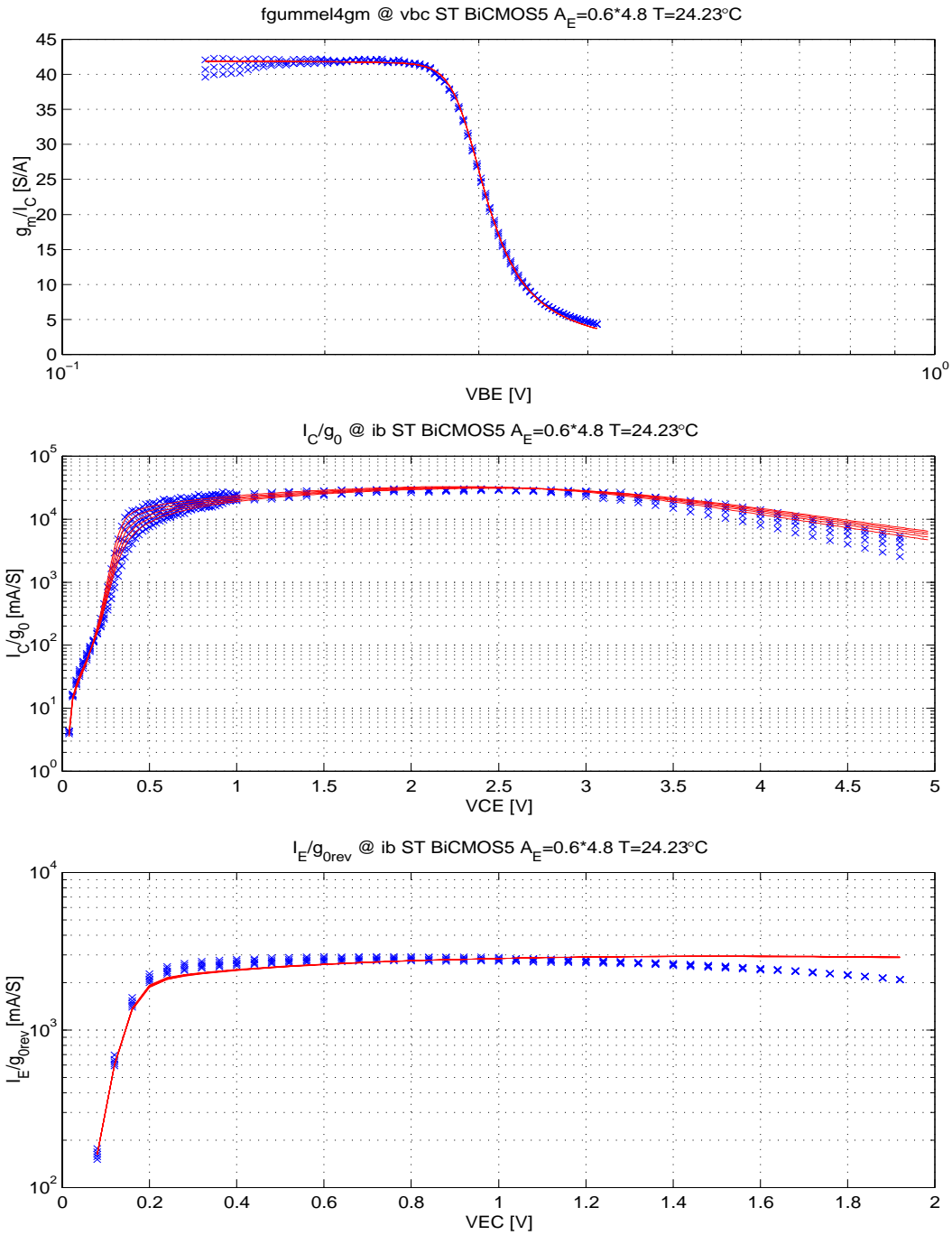


Fig. 1.4/7: Normalized transconductance vs.  $V_{BE}$ ; forward and reverse “Early voltage”.

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'*' HICUM / LEVEL2 DC-Satz
'MODQ' 'Tref' 1
&HICUM2 c10=4.78E-32 qp0=2.25E-14 ich=5.60E-03 hfc= 0.20
hfe= 1.00 hpci= 0.68 hpei= 1.00 alit=0.450
cpei0=8.88E-15 vpei=0.960 ze=0.595 alpe= 2.20
cpci0=2.12E-15 vpci=0.780 zci=0.474 vptci=1.05E+01
t0=1.03E-11 dt0h=-1.170E-12 tbvl=5.300E-13 tef0=2.55E-13
gtfe= 1.00 thcs=3.16E-11 alhc= 8.143 fthc= 0.800
alqf=0.225
rci0=3.61E+01 vlim= 0.387 vpt= 4.19 vces= 0.100
tr=0.00E+00
ibeis=1.96E-20 mbei=1.0080 ireis=7.00E-17 mrei=2.0000
ibcis=1E-30 mbci=1.0240
favl= 03.0 qavl=4E-14
rbi0= 125.50 fdqr0=0.200 fgeo=0.7570 fqi=1.0000
fcrbi=0.20
latb=3.470E+00 latl=0.434
cjep0=7.95E-15 vdep=0.980 zep=0.437 aljep= 2.30
ibeps=1.00E-30 mbep=1.0110 ireps=1.00E-30 mrep=2.0000
ibets=0.00E+00 abet= 0.00
cjcx0=1.42E-14 vdcx=0.835 zcx=0.452 vptcx=2.30E+00
ccox=2.78E-15 fbc=0.128
ibcx=13E-18 mbcx=1.043
ceox=1.13E-15 rbx= 31 re= 15.500 rcx= 6
itss=1.00E-30 msf=1.000 tsf=0.00E+00
iscs=1.00E-30 msc=1.000
cjs0=4.01E-14 vds=0.650 zs=0.282 vpts=1.00E+03
rsu= 0.0 csu=0.00E+00
kf=0.00E+00 af=1.00E+00
vgb= 1.160 alb= 1.60E-04 alt0= 0.00E+00 kt0= 0.00E+00
zetaci= 1.600 alvs=1.00E-03 alces=4.00E-04 zetarbi= 0.830
zetarbx= 0.180 zetarcx= 0.190 zettare= -0.800
alfav=8.25E-05 alqav=1.96E-05
rth= 400.00 cth=0.00E+00 &end

```

Fig. 1.4/8: Set of model parameters for the DC measurement based comparison (DEVICE).