
Charge partitioning of the intrinsic HBT according to the TICCR

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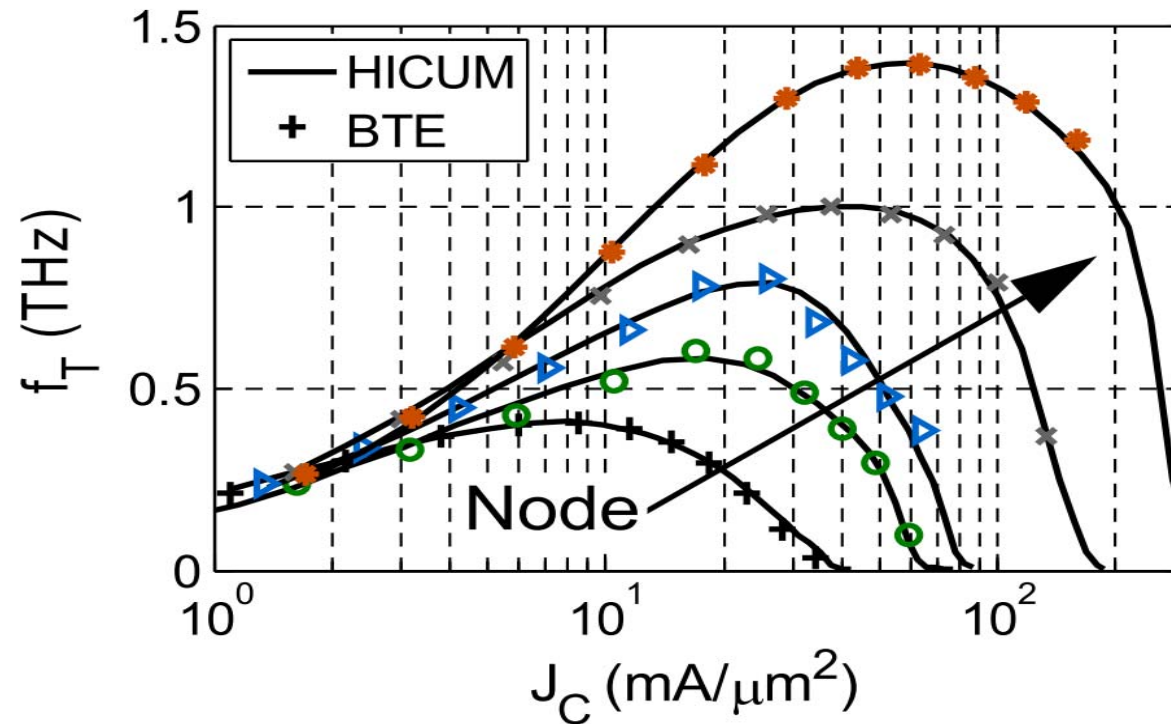
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Introduction

Motivation of this work



Modeling in the terahertz gap?

Predictions of dynamic behavior of charges on physical basis necessary!

- [1] M. Schröter, T. Rosenbaum, P. Chevalier, B. Heinemann, S. P. Voinigescu, E. Preisler, J. Böck, and A. Mukherjee, „SiGe HBT technology: Future trends and TCAD-based roadmap”, Proc. of the IEEE, vol. 105, no. 6, pp. 1068-1086, 2017.

The Transient Integral Charge-Control Relation (TICCR)

- TICCR [2] yields closed-form analytical solution for 1D current densities:

$$j_C(t) = j_T(t) - q \int_0^{x_{bl}} \eta_C \left(R + \frac{\partial n}{\partial t} \right) dx$$

$$j_E(t) = j_T(t) + q \int_0^{x_{bl}} \eta_E \left(R + \frac{\partial n}{\partial t} \right) dx$$

- common transfer current component equal to GICCR (except for h_f)

$$j_T(t) = qV_T \mu_{nr} n_{ir}^2 \frac{\exp\left(\frac{V_{B'E'}}{V_T}\right) - \exp\left(\frac{V_{B'C'}}{V_T}\right)}{\int_0^{x_{bl}} h_v h_g p dx}$$

=> can be directly applied to HICUM

=> Focus here on time dependent terms of TICCR current density

- [2] H. Klose and A. Wieder, „The transient integral charge control relation: A novel formulation of the currents in a bipolar transistor," IEEE Trans. Electron Dev., vol. 34, no. 5, pp. 1090-1099, 1987.

Charge partitioning

- partitioning functions:

$$\eta_C(t) = \frac{\int_0^x h_v h_g p d\xi}{\int_0^{x_{bl}} h_v h_g p dx}$$

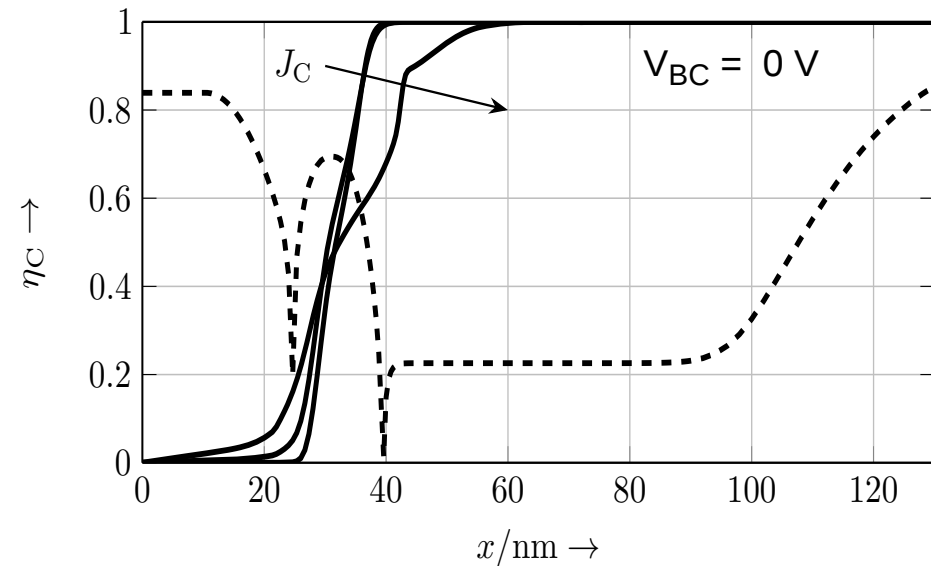
$$\eta_E(t) = 1 - \eta_C$$

with GICCR weight functions

$$h_v(t) = \exp\left(\frac{v_{B'E'}(t) - \phi_p(x, t)}{V_T}\right). \quad h_g(t) = \frac{\mu_{nr} n_{ir}^2}{\mu_n(x, t) n_i^2(x)}$$

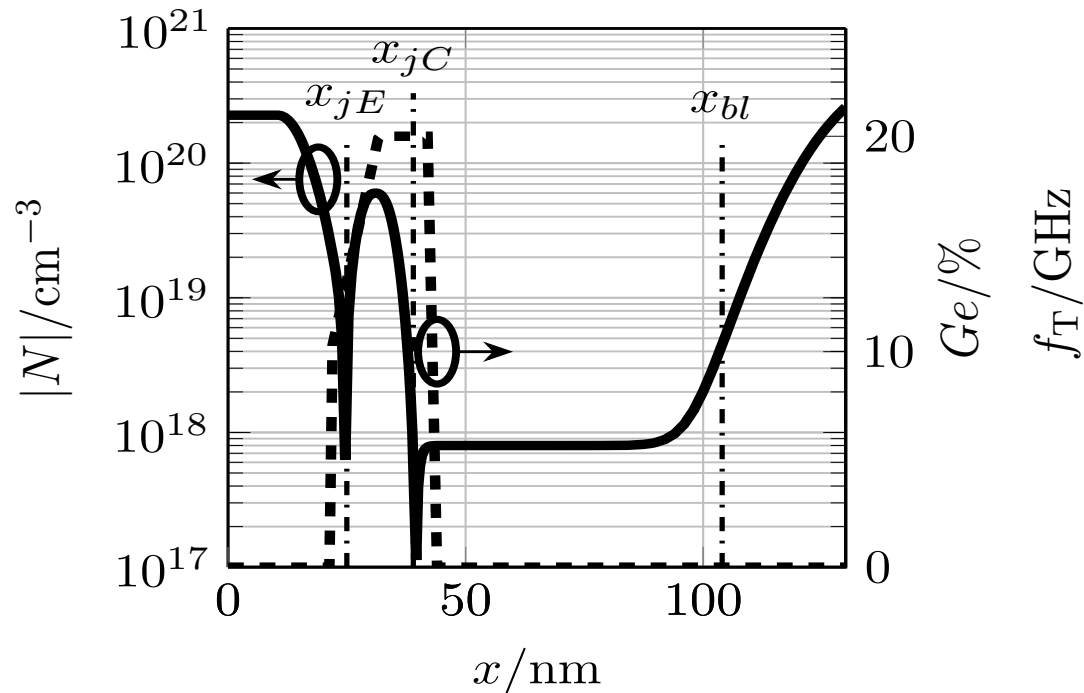
=> η_C (η_E) determines fraction of charge that is supported by C (E) terminal during dynamic operation

- weak bias dependence up to medium J_C

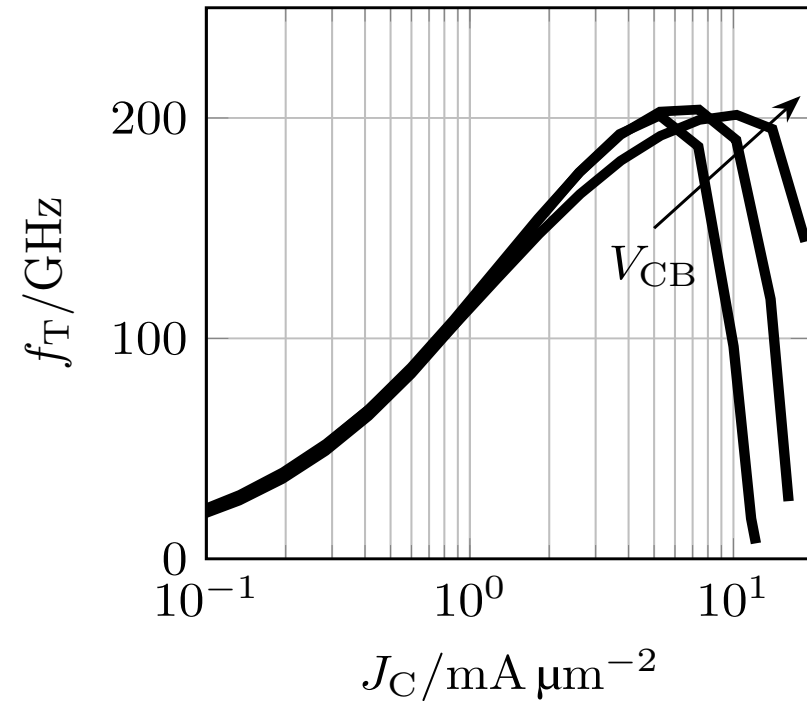


Selected transistor structure

1D doping profile [3]



transit frequency

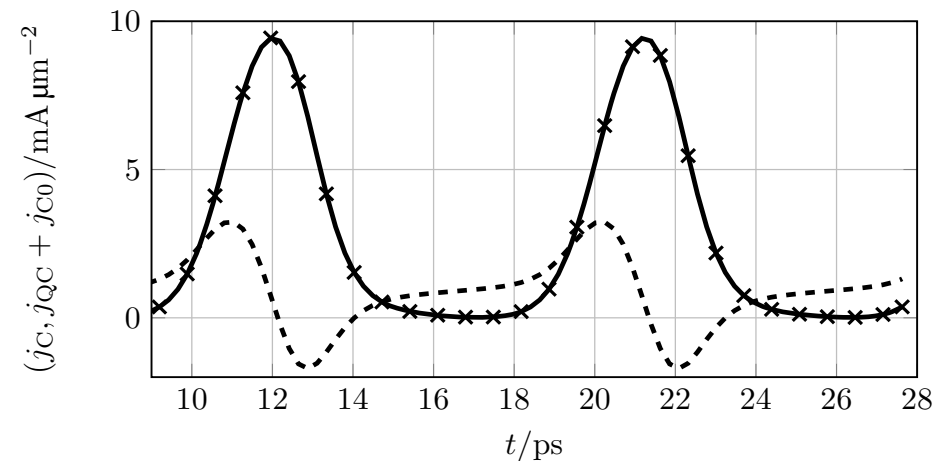
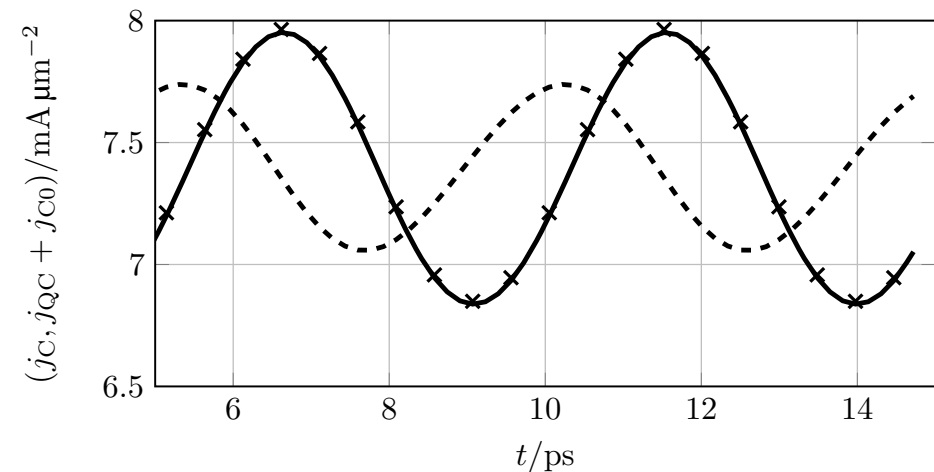


- Integration limits of the TICCR according to [3]
- DD transport dominant
 - for more advanced structures => use augmented DD transport

[3] M. Schroter, S. Lehmann, and A. Pawlak, „Why is there no internal collector resistance in HICUM?", IEEE Bipolar/BiCMOS Circ. and Technol. Meeting (BCTM), pp. 142-145, 2016.

Comparison of TICCR with device simulation

- sinusoidal monofrequent input signal with frequency f
- small-signal operation
 - OP: $(J_C, V_{BC}) = (7.39 \text{ mA}/\mu\text{m}^2, 0 \text{ V})$
 $\Rightarrow$ peak f_T
 - $f = 203 \text{ GHz}$ (= peak f_T)
 - 2.5 mV V_{BE} amplitude
- large-signal operation
 - OP: $(J_C, V_{BC}) = (1.26 \text{ mA}/\mu\text{m}^2, 0 \text{ V})$
 - $f = f_T = 131 \text{ GHz}$
 - 70 mV V_{BE} amplitude
 - $\Rightarrow \max. j_C(t) = 1.5 J_C(f_{T,\text{peak}}) !$



- excellent agreement for small-signal and large-signal case
 $\Rightarrow$ reference for compact model related simplifications

Compact modeling approach

Simplifications of TICCRR charge description

Assumptions

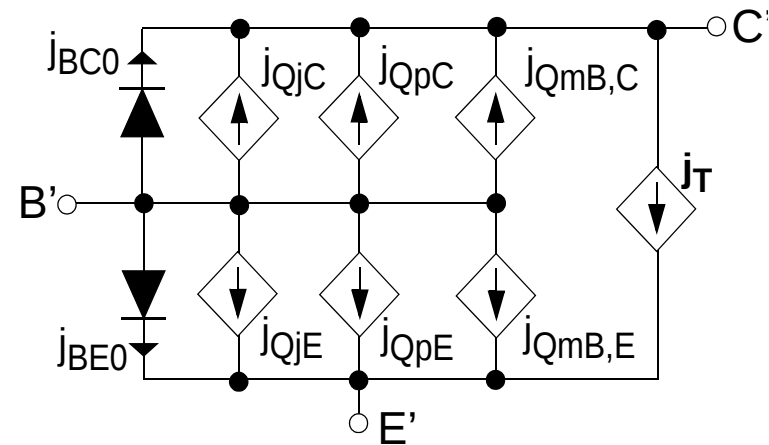
- quasi-static carrier distribution => charge, GICCR
- negligible recombination => collector charging current density:

$$j_{QC} = q \int_0^{x_{bl}} \eta_C \frac{\partial n}{\partial t} dx$$

- $\eta_C = 1$ for BC region => components

$$j_{QjC} = \frac{\partial \bar{Q}_{jC}}{\partial t} = q \int_{x_{jC}}^{x_{bl}} \frac{\partial (\Delta n - \Delta p)}{\partial t} dx$$

$$j_{QpC} = \frac{\partial \bar{Q}_{pC}}{\partial t} = q \int_{x_{jC}}^{x_{bl}} \frac{\partial \Delta p}{\partial t} dx$$



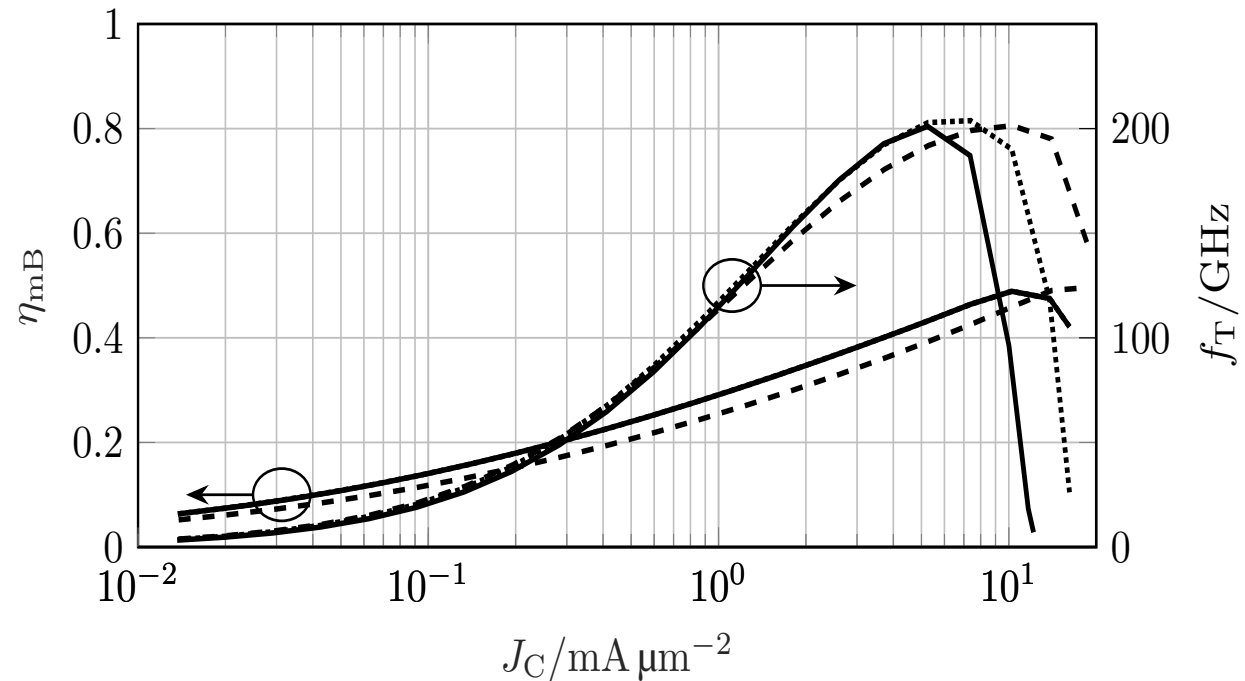
- assume $\eta_C = \eta_{mB} < 1$ for base region only:

$$j_{QmB,C} = \eta_{mB} \frac{\partial \bar{Q}_{mB}}{\partial t} \quad \text{with} \quad \eta_{mB} = \int_{x_{jE}}^{x_{jC}} \eta_C \Delta n dx / \int_{x_{jE}}^{x_{jC}} \Delta n dx$$

Base charge partitioning factor

$$\eta_{mB} = \frac{\int_{x_{jE}}^{x_{jC}} \eta_C \Delta n dx}{\int_{x_{jE}}^{x_{jC}} \Delta n dx}$$

- $V_{BC}/V = 0.5, 0 (\dots), -1.2 (- -)$
- f_T curve added for reference

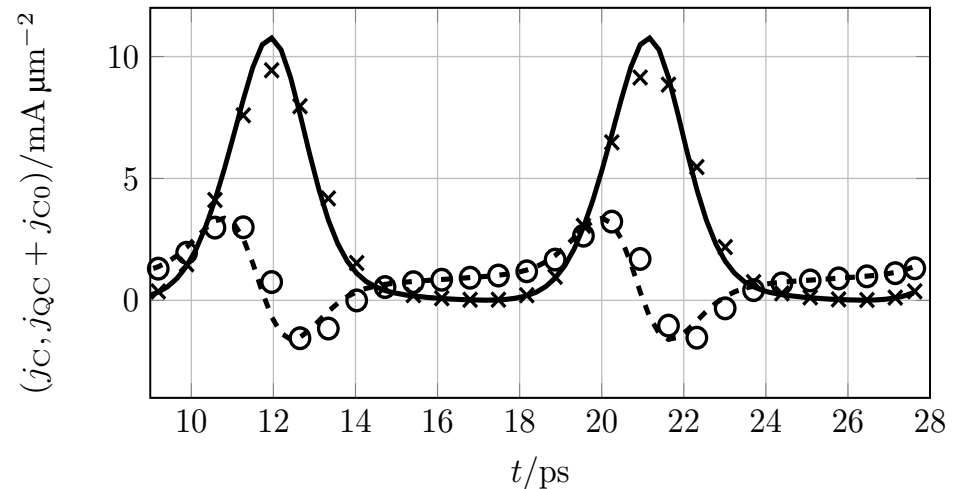
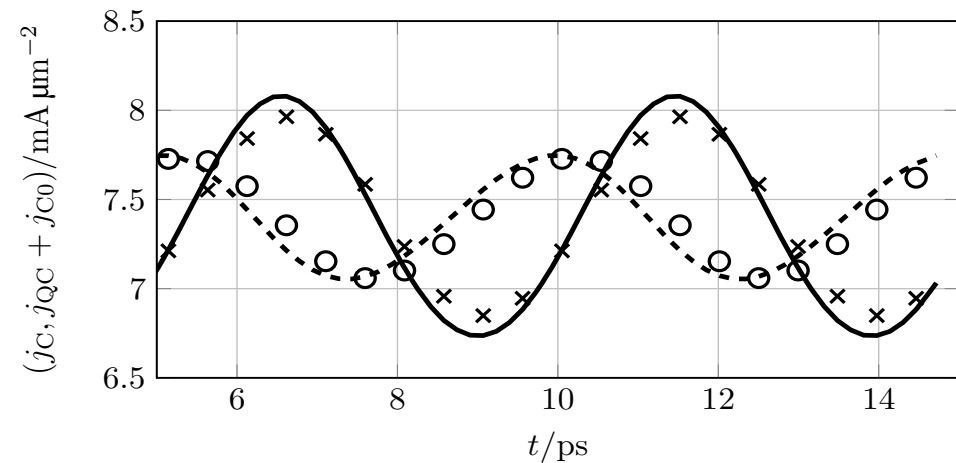


$\Rightarrow \eta_{mB}$ depends on J_C , but only slight function of V_{BC}

- analytical formulation for bias dependence yet to be developed
 - excess phase shift = $\text{atan}(\omega \eta_{mB} C_{dE} / g_m) = \text{atan}(\omega \eta_{mB} \tau_f) \Rightarrow \eta_{mB} = \alpha_{IT}$
- **existing compact models use bias independent partitioning factor** (e.g. **fixed value 1/3** in MEXTRAM)

Comparison to device simulation

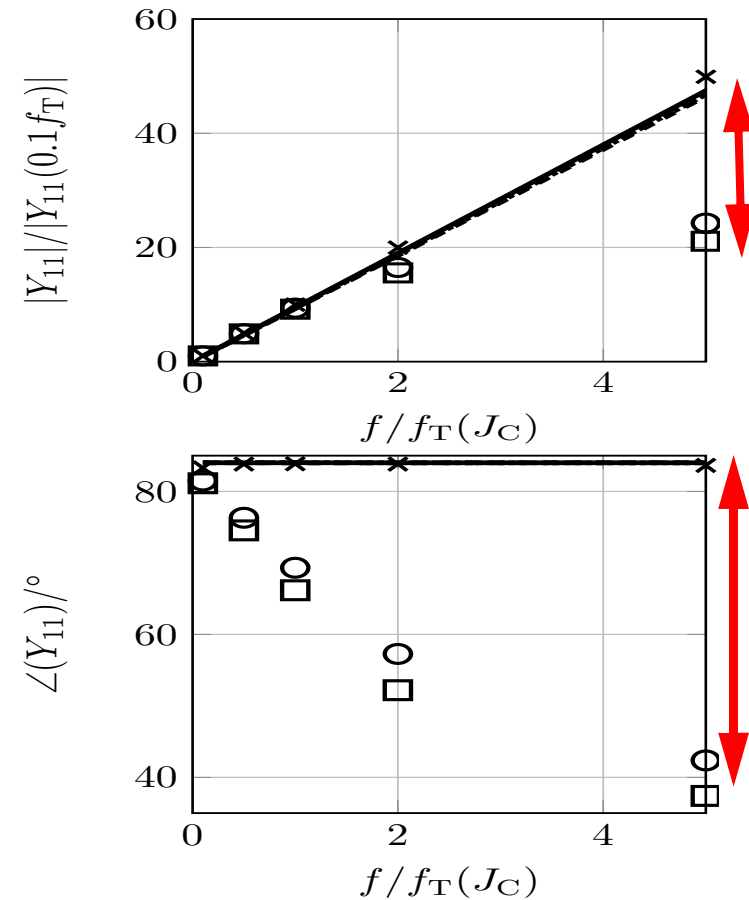
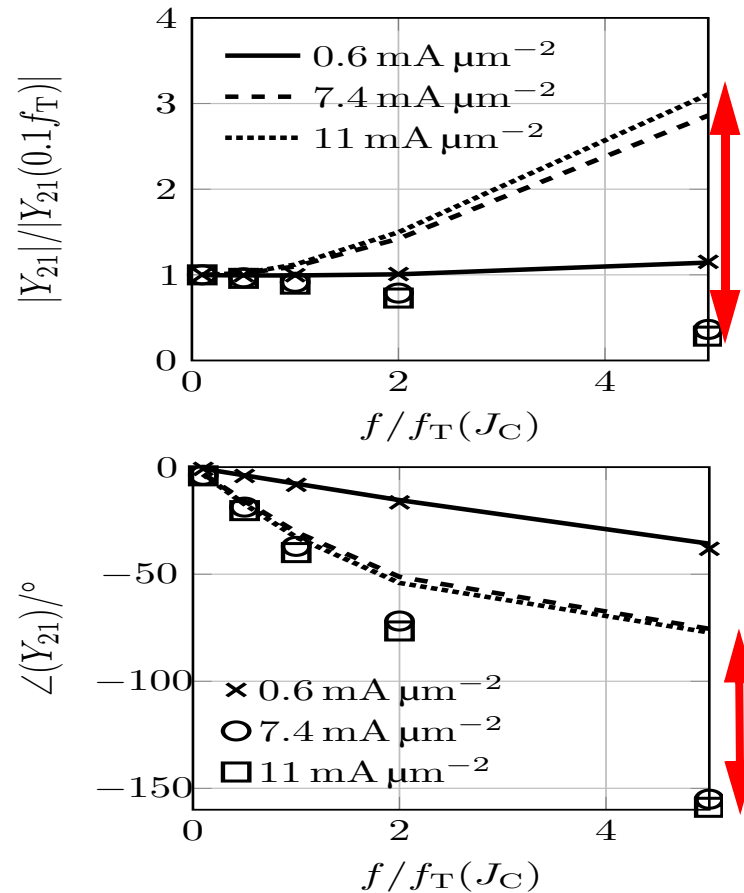
- sinusoidal monofrequent input signal with frequency f
=> same conditions as before
- small-signal operation: model ...
 - amplitude higher
 - phase shifts
- large-signal operation: model ...
 - amplitude overshoot
 - phase shift during turn-off
- causes for deviations?
 - dynamic j_C component phase shift
 - other?



=> **charge partitioning alone is not sufficient for accurately capturing dynamic collector terminal current!**

Frequency domain results

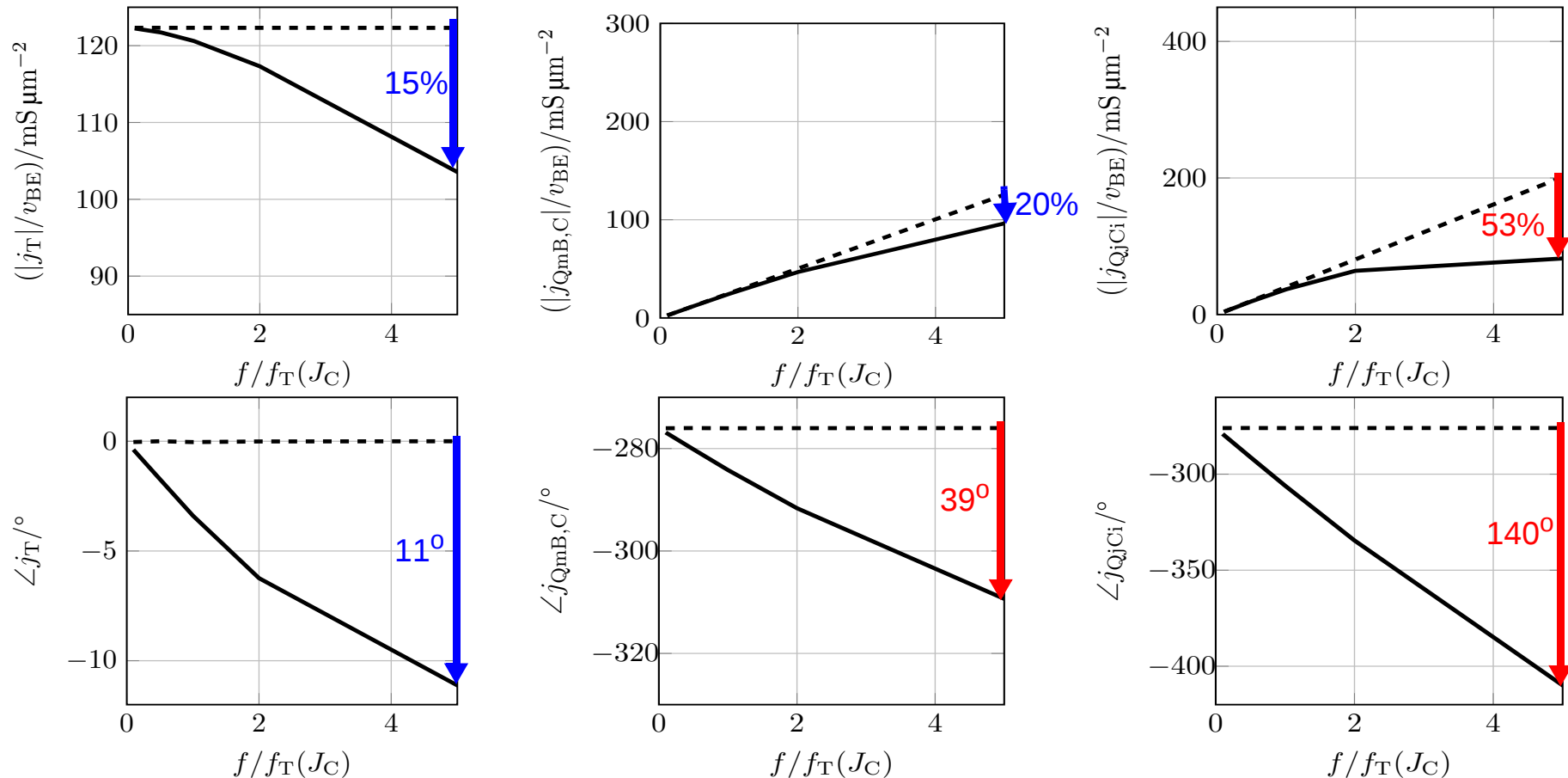
...indicating cause of observed deviations



- accurate at low forward bias, but significant deviations at high bias
 => charge partitioning misses phase shift in **mobile** charge!

Deviations at higher harmonics

comparison of TCAD vs. CP model with charges from **q.s.** simulation



- relatively weak frequency dependence of transfer current
- **significant frequency dep. of BC depletion charge (SCR modulation!)**

Summary

- TICCR offers exact solution of drift-diffusion-based charging currents
=> use as reference for 1D compact model development
- Using quasi-static charges, TICCR based charge-partitioning shows high accuracy up to $f_{T,1D}$, but large deviations for harmonics from $2 f_{T,1D}$ on
- Base charge partitioning factor depends on J_T
=> charge-partitioning model must include phases of charges!

Outlook

- Measurements of HV devices to validate predictions experimentally
- Develop (i) bias dependent base charge partitioning factor and (ii) representation of additional phase shift in BC depletion current
- Replace gyrator adjunct EC in HICUM by new analytical charge partitioning
=> allows to delete two nodes
=> runtime reduction!

Acknowledgments

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